

Modal-based Damage Localisation

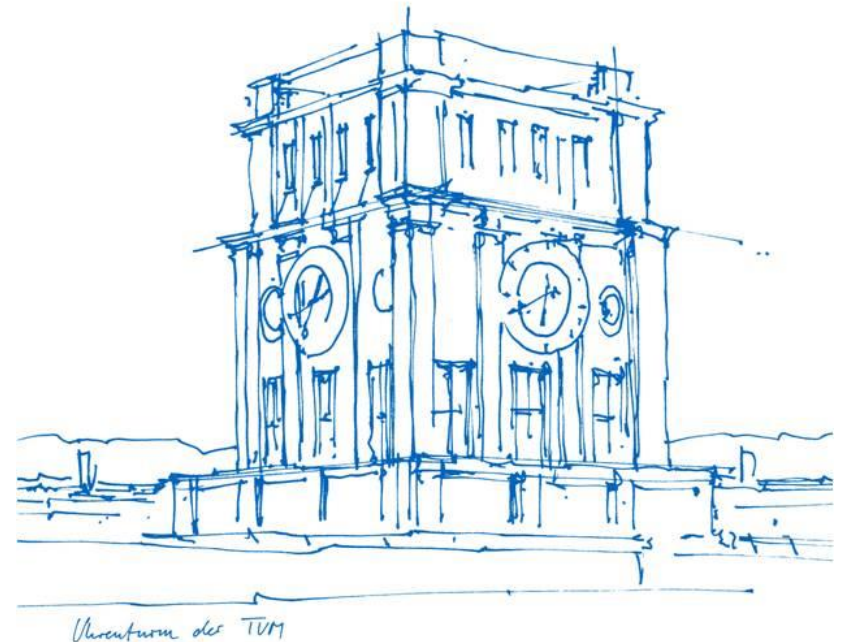
BGCE research day Presentation

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Outline

- **Part1 Introduction:** Damage Localisation + Modal based
- **Part2 Workflow:**
 - benchmark tool to define a simulated damage
 - generate sensor-like data
 - try out different damage Index
 - assess damage
- **Part3 Damage assessment**
- **Part4 Summary**

Part1 Introduction: Modal-based Damage Localisation

Structure Health Monitoring = Damage Identification :

1. Four levels:

- 1). Detection (Does the damage exist?)
- 2). Localisation (Where is the damage?)
- 3). Classification & quantification (What type the damage is ? & how severe it is?)
- 4). Prediction (How long will the structure survive? What actions will we take?)

2. Two approaches: Choose a damage sensitive feature (DSF):

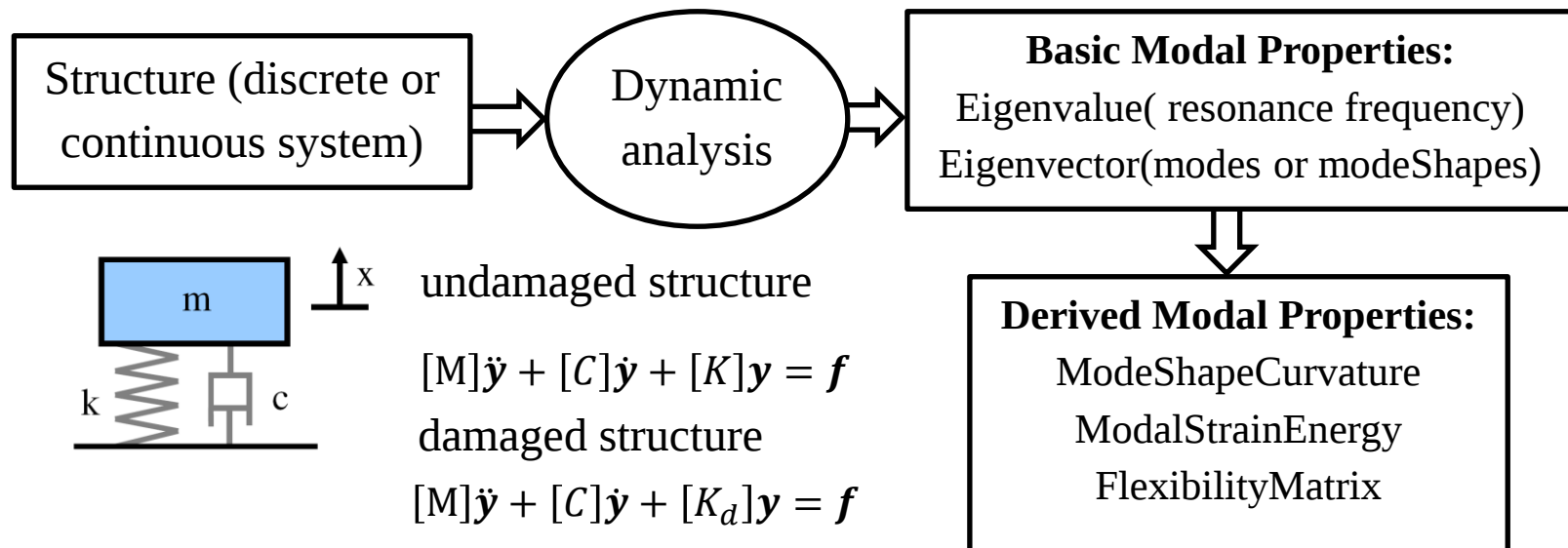
- Model-based approach (inverse-problem approach):
 - physical-based model (e.g. a FE model). First build a model, then update it using the measured datas from the real structure. Damage Index can be chosen as features from basic [modal properties](#)
- Data-based approach :
 - not based on a law-based model but a statistical model (e.g. a probability density function) from training data. Then use the pattern recognition to find the damage Index.

3. Several Axioms¹:

- Damage can not be directly measured (Acclerations, strains, even modes-related datas can be measured)
- Damage assessment required a comparison between two system states ...

Part1 Introduction: **Modal**-based Damage Localisation

Modal analysis:



Damage(**stiffness reduction**): $[K] \rightarrow [K_d]$, $[M] \rightarrow [M]$, $[C] \rightarrow [C]$

Part 2 Workflow: Damage Settings explanation

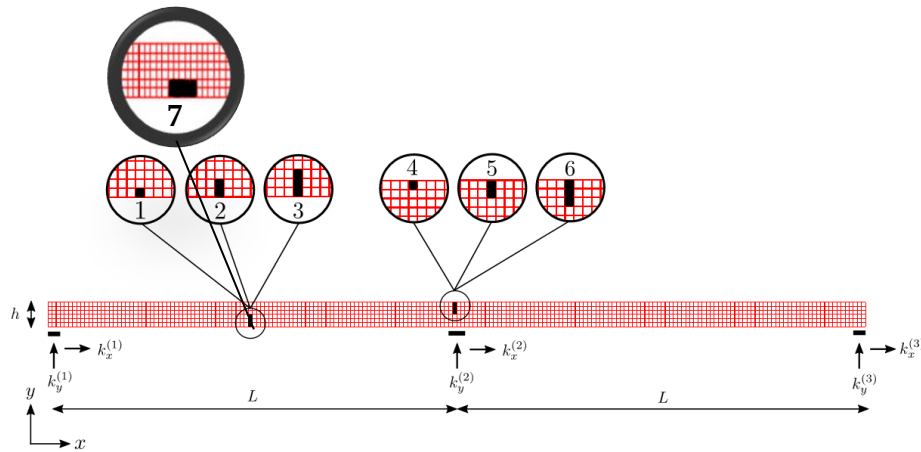


Figure 1: Finite element model of the benchmark structure.

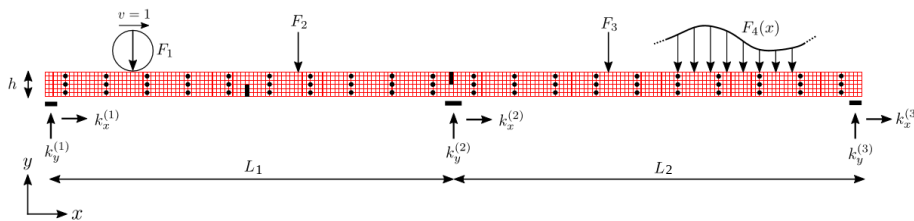


Figure 2: Load cases and measurement positions

Geometry: $L_1 = 12, L_2 = 13, h = 0.6, w = 0.1$

FEM model: isoparametric quadrilateral elements for plane-stress problem with predefined 200×6 elements.

$$dx = 25/200 \quad dy = 0.6/6$$

Material assumption: linear elastic material with $E = 30e10$, poisson ratio $\gamma = 0.3$, material density $\rho = 7800$

E is reduced by 20%, 50%, 70% at the predefined location. Here we study the case when one damage appears in the structure. Damaged7(enlarged damaged 2)

Boundary Condition: Here only $F_4(x)$ the distributed loads modeled as independent Gaussian white noise is applied.

Sensor Location: 60 sensors is predefined in the simulator, each sensor can return the value (either accelerations or modes) in x, y directions

$$\text{deltax} = 10 * dx (20 \text{ sensors})$$

$$\text{deltay} = 20 * dx (10 \text{ sensors})$$

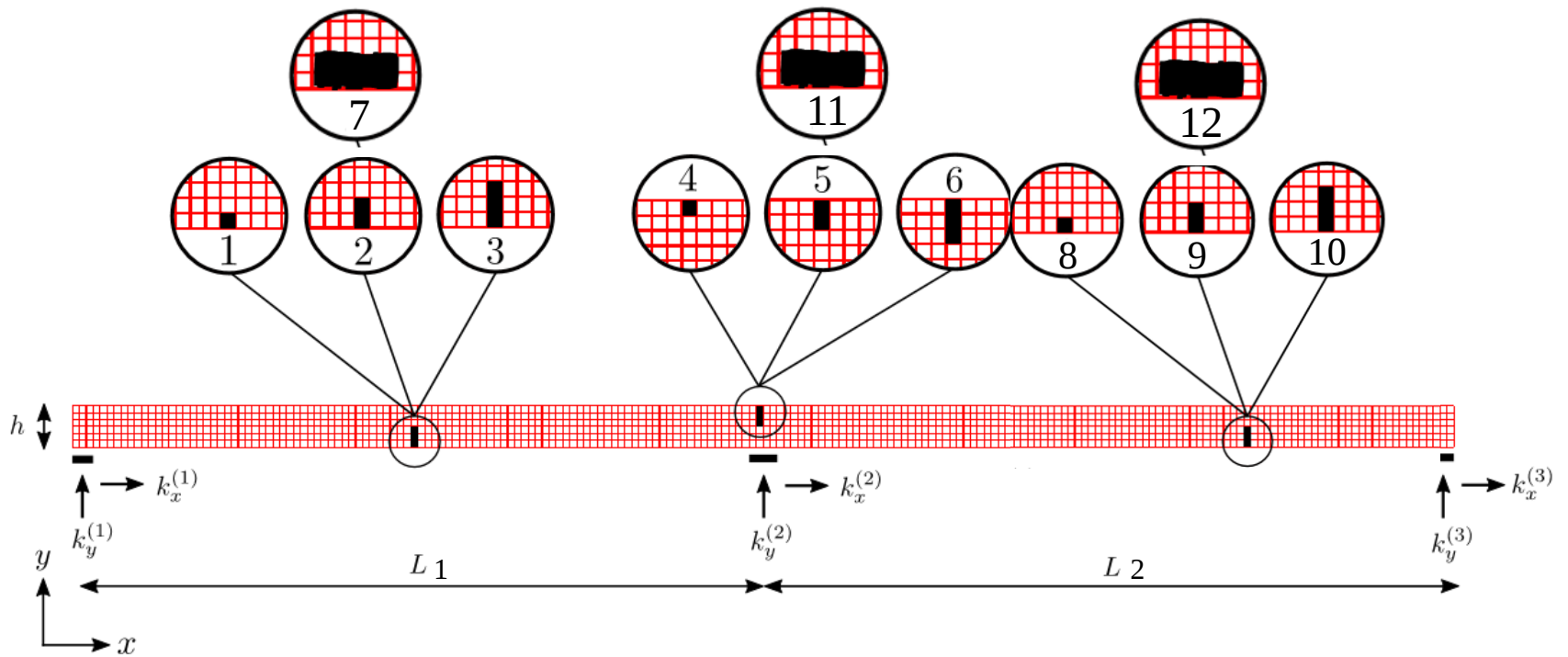
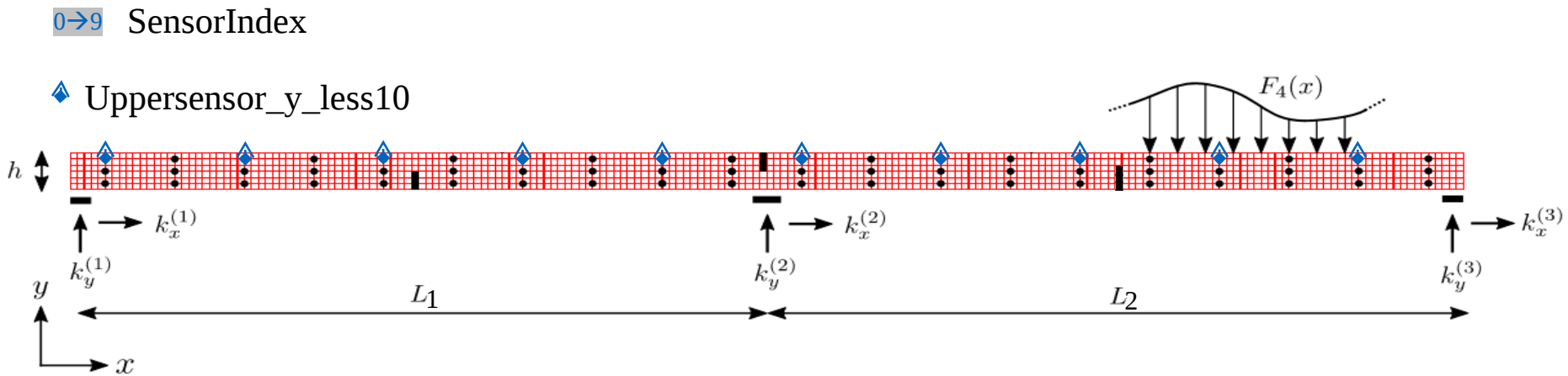
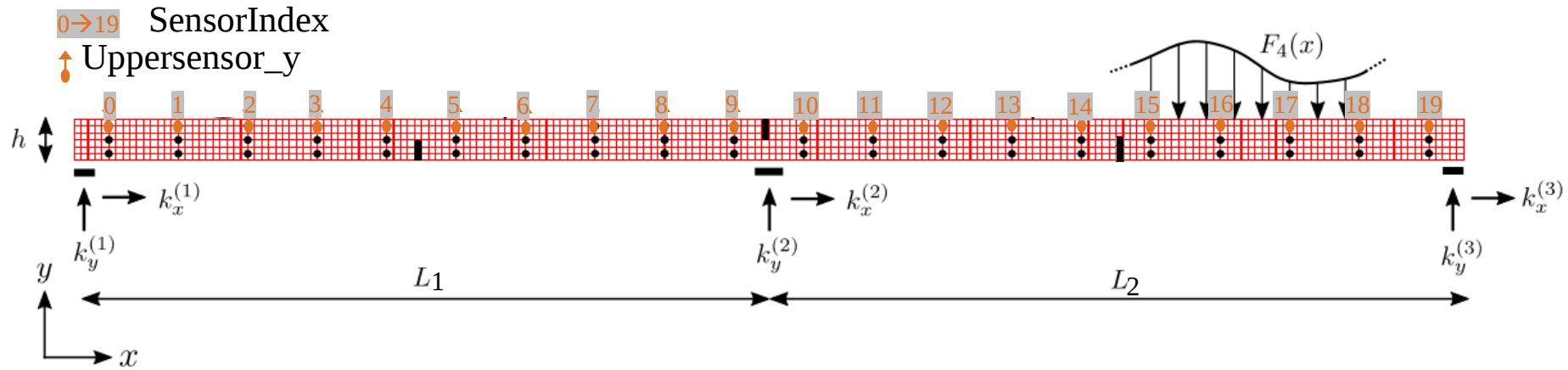
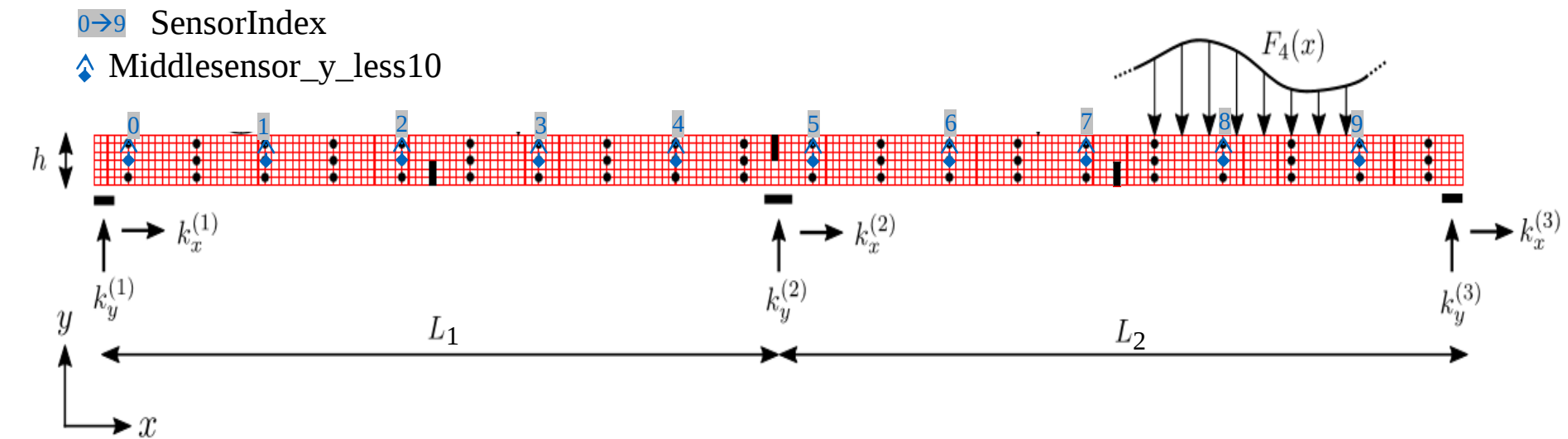
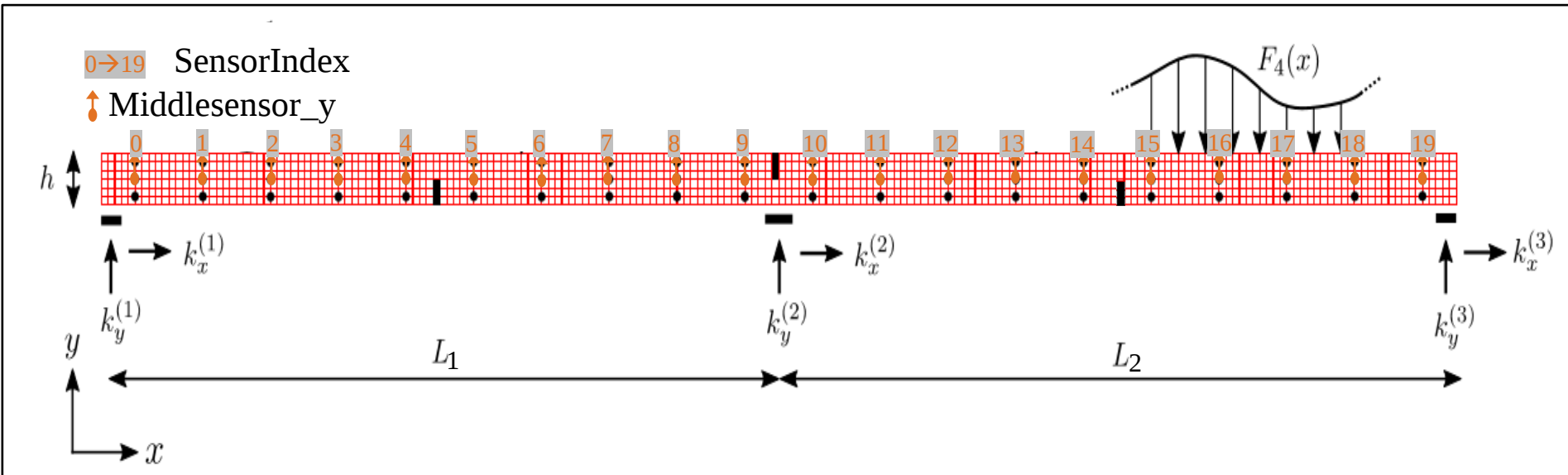
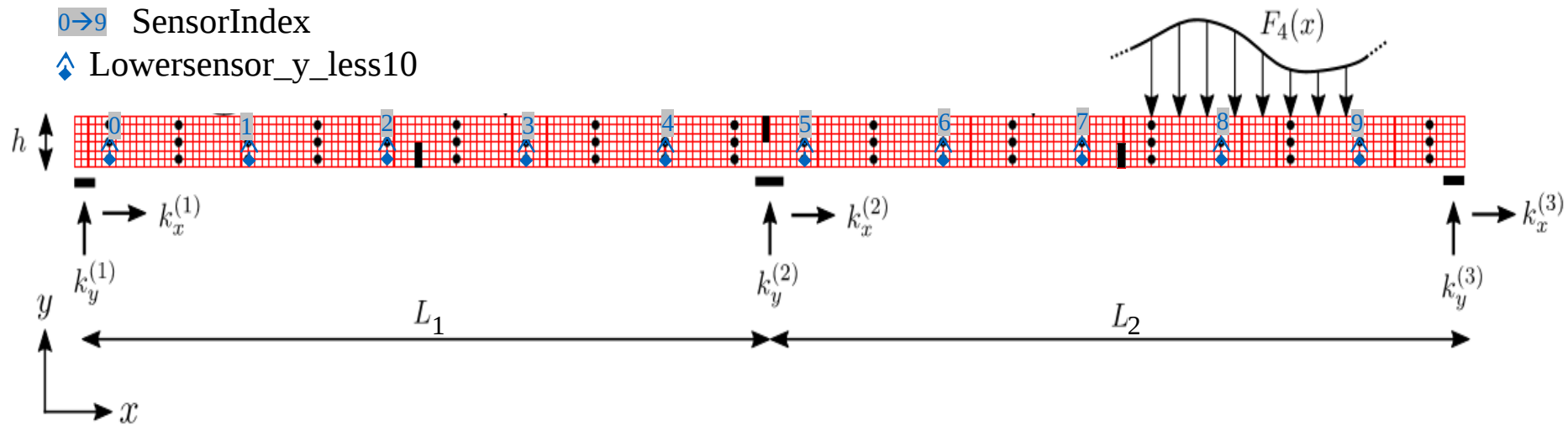
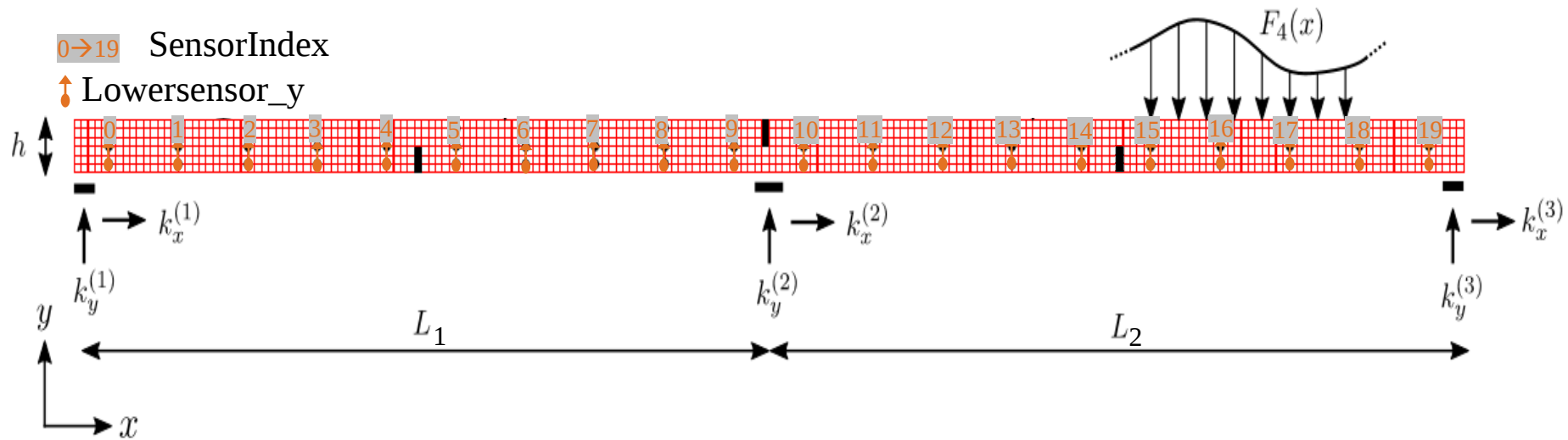


Figure 1: Finite element model of the benchmark structure.







Combine the sensor and damage settings

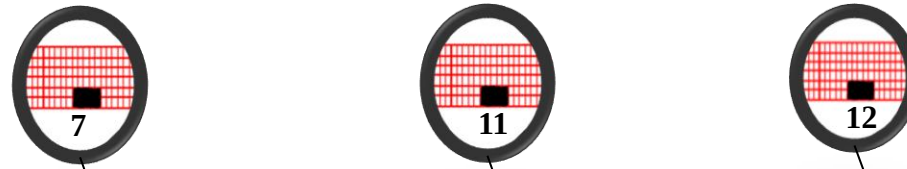


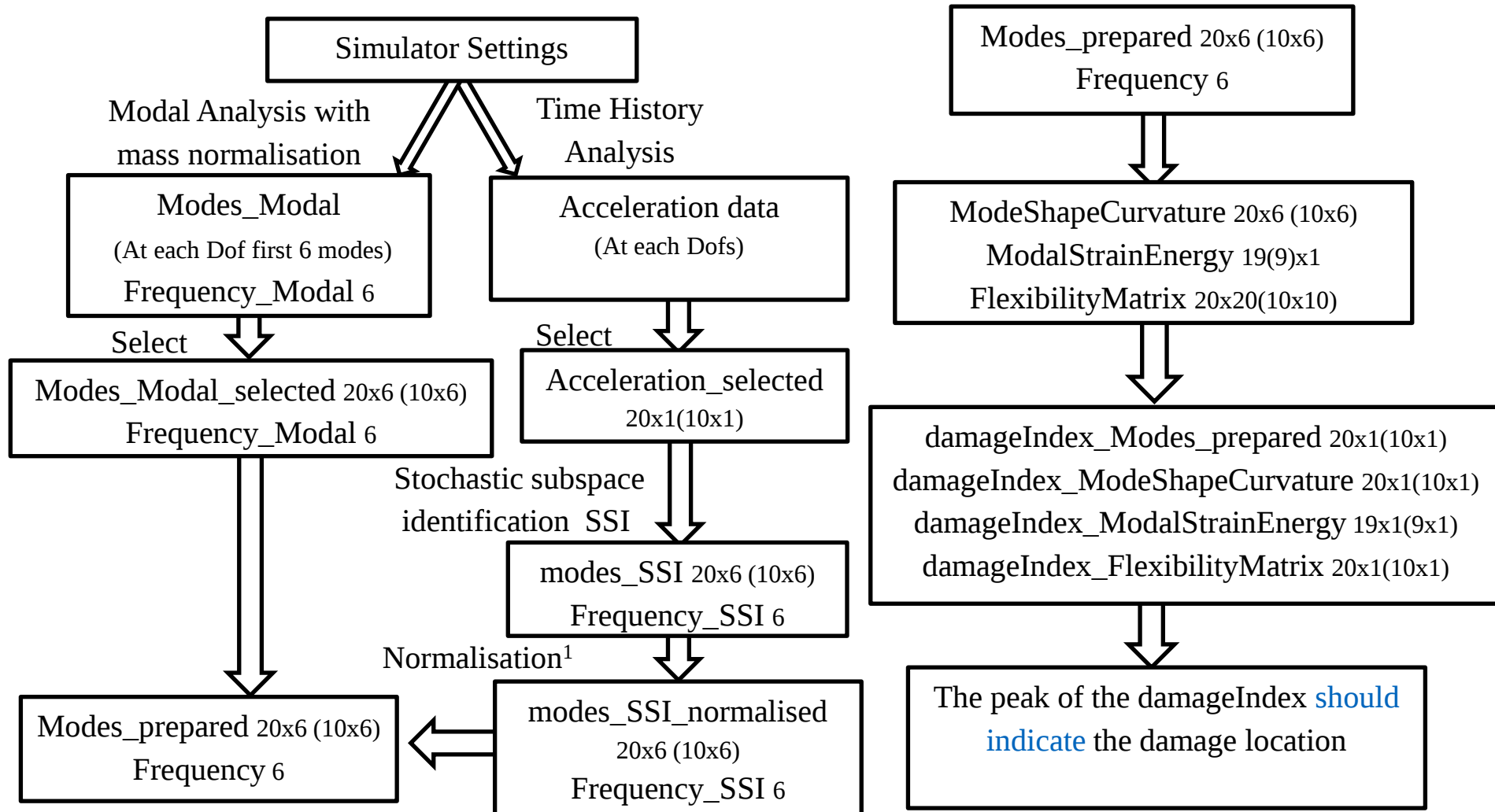
Table1 20 Sensors index

Region Index		0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	
Sensor Index	Uppersensor_y	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	Middlesensor_y																				
	Lowersensor_y																				
x (*dx)	dx = 25/200	5	15	25	35	45	55	65	75	85	95	105	115	125	135	145	155	165	175	185	195

Table2 10 Sensors index

Region Index		0		1		2		3		4		5		6		7		8	
Sensor Index	Uppersensor_y_less10	0	1	2	3	4	5	6	7	8	9								
	Middlesensor_y_less10																		
	Lowersensor_y_less10																		
x (*dx)	dx = 25/200	5	25	45	65	85	105	125	145	165	185								

Part 2 Workflow summary



Part 3 Damage assessment: **damageIndex** overview

To define a damage index, we need to find the damage sensitive features (DSF)

And we know that damage assessment is between two states, we need to make an appropriate **mathematical operations** to see the difference between healthy and unhealthy state:

#Subtraction $\text{DamageIndex} = \text{DSF}_{\text{damaged}} - \text{DSF}_{\text{undamaged}}$

1. $\text{DamageIndex_absdiff} = \text{abs}(\text{DSF}_{\text{damaged}} - \text{DSF}_{\text{undamaged}})$

2. $\text{DamageIndex_absabsdiff} = \text{abs}(\text{abs}(\text{DSF}_{\text{damaged}}) - \text{abs}(\text{DSF}_{\text{undamaged}}))$

3. $\text{DamageIndex_abssqudiff} = \text{abs}((\text{DSF}_{\text{damaged}})^2 - (\text{DSF}_{\text{undamaged}})^2)$

#Division

$$\text{DamageIndex_division} = \frac{\text{DSF}_{\text{damaged}}}{\text{DSF}_{\text{undamaged}}}$$

Part 3 Damage assessment :DamageIndex basic modal Features

Frequency
:

Frequency_Modal	undamaged	damaged7_20%	damaged7_50%	damaged7_70%
1st	7.6763	7.6698	7.6532	7.6309
2nd	9.3719	9.3555	9.3156	9.2661
3rd	19.5276	19.5261	19.5224	19.5177
4th	23.4582	23.4565	23.4524	23.4470
5th	34.1261	34.0891	33.9953	33.8713
6th	38.2315	38.1934	38.1017	37.9909

Mode
shape:

Frequency_SSI	undamaged	damaged7_20%	damaged7_50%	damaged7_70%
1st	7.6797	7.6686	7.6488	7.6234
2nd	9.3689	9.3500	9.3150	9.2689
3rd	19.5221	19.5127	19.5146	19.5095
4th	23.4183	23.4466	23.4106	23.4064
5th	34.0940	33.9948	33.9075	33.7713
6th	38.1451	38.1160	37.9812	37.8777

Frequency_SSI_less10	undamaged	damaged7_20%	damaged7_50%	damaged7_70%
1st	7.6797	7.6686	7.6488	7.6234
2nd	9.3689	9.3500	9.3150	9.2689
3rd	19.5221	19.5127	19.5146	19.5095
4th	23.4183	23.4466	23.4105	23.4064
5th	34.0947	33.9948	33.9078	33.7713
6th	38.1466	38.1153	37.9802	37.8787

Part 3 Damage assessment :DamageIndex basic modal Features

Frequency:

Mode shape:

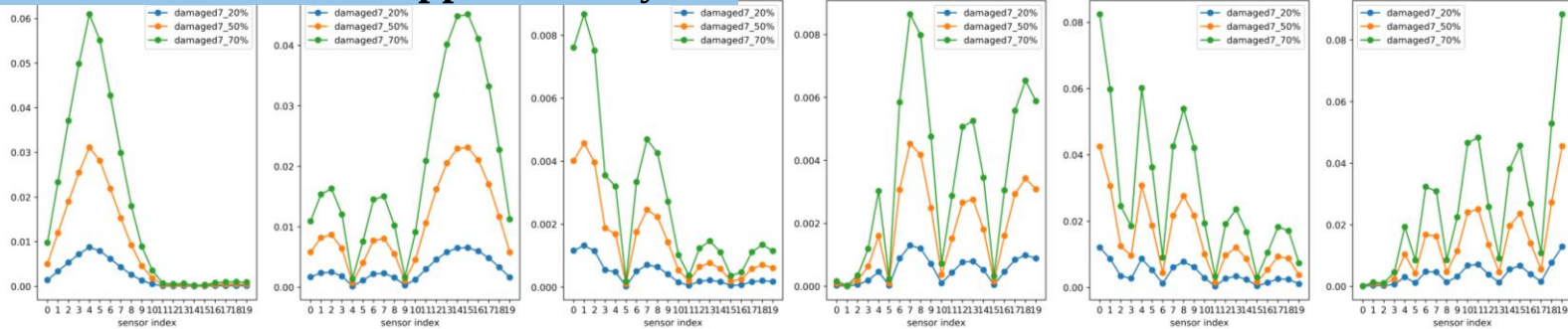
Modes_Modal(modes_SSI):

```

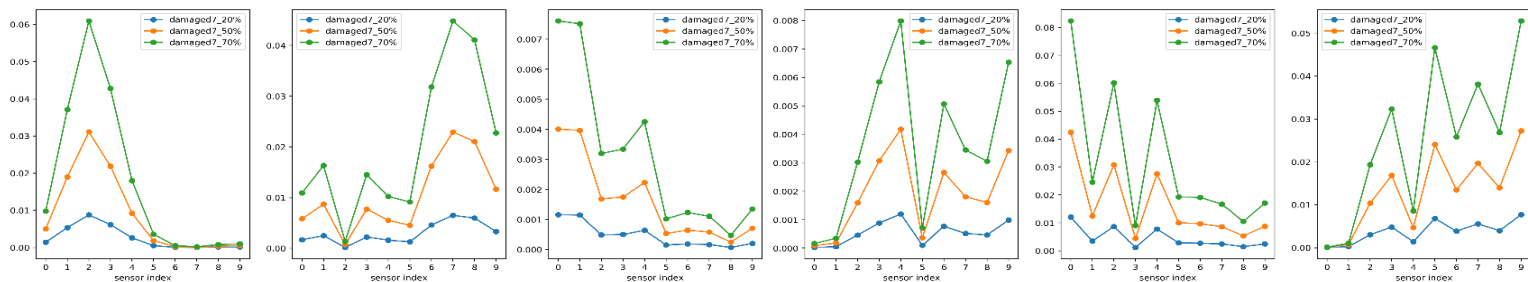
absdiff⊗⊗⊗ absdiff=abs(DSFdamaged − DSFundamaged)
    #each order
        #Uppersensor_y(20sensors) #Uppersensor_y_less10(10sensors)
    #Sum of all order
        #Uppersensor_y(20sensors) #Uppersensor_y_less10(10sensors)
    #Sum of first two orders
        #Uppersensor_y(20sensors) #Uppersensor_y_less10(10sensors)
absabsdiff⊗ absabsdiff=abs(abs(DSFdamaged) − abs(DSFundamaged))
    #each order
        #Uppersensor_y(20sensors) #Uppersensor_y_less10(10sensors)
    #Sum of all order
        #Uppersensor_y(20sensors) #Uppersensor_y_less10(10sensors)
    #Sum of first two orders
        #Uppersensor_y(20sensors) #Uppersensor_y_less10(10sensors)
abssqudiff⊗ abssqudiff=abs((DSFdamaged)2 − (DSFundamaged)2)
    ....

```

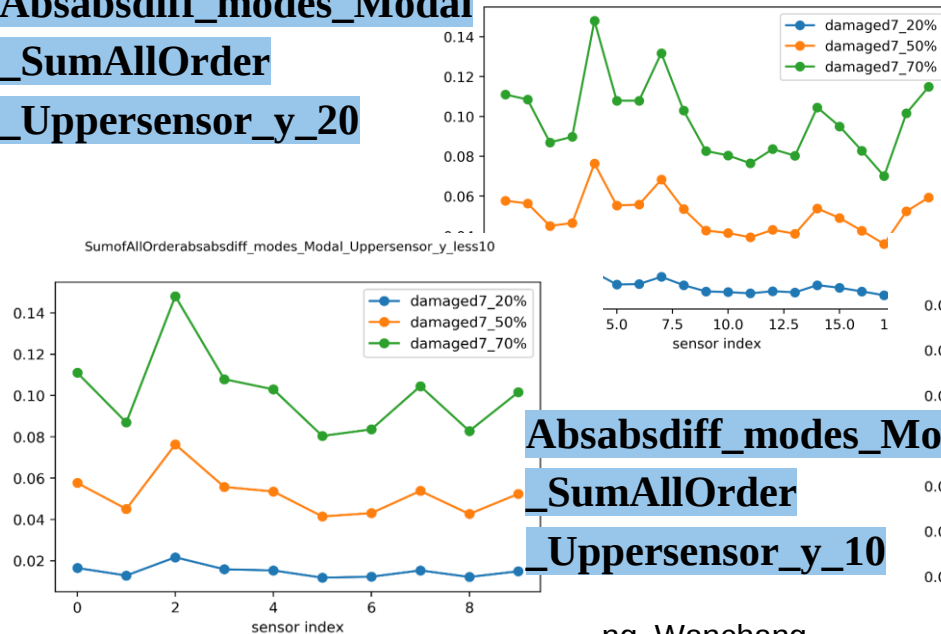
Absabsdiff_modes_Modal_eachorder_Uppersensor_y_20



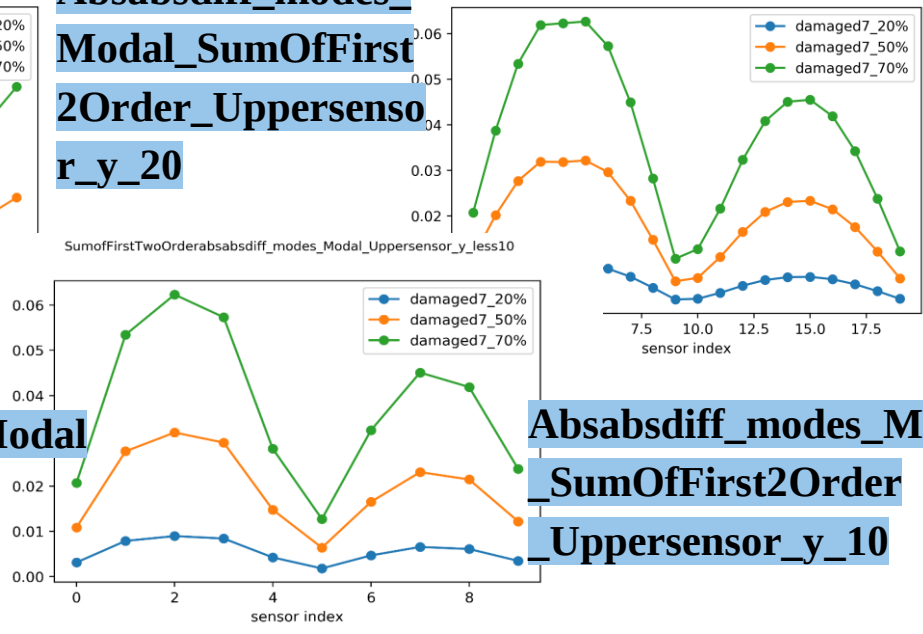
Absabsdiff_modes_Modal_eachorder_Uppersensor_y_10



Absabsdiff_modes_Modal_SumAllOrder_Uppersensor_y_20



Absabsdiff_modes_Modal_SumOfFirst2Order_Uppersensor_y_20



Absabsdiff_modes_Modal_SumAllOrder_Uppersensor_y_10

Absabsdiff_modes_Modal_SumOfFirst2Order_Uppersensor_y_10

Part 3 Damage assessment :DamageIndex derived modal Features

ModeShapeCurvature: (2nd order derivative of modeShape)

The middle points use the central difference scheme to get the 2nd ModeShapeCurvature

Middle points:

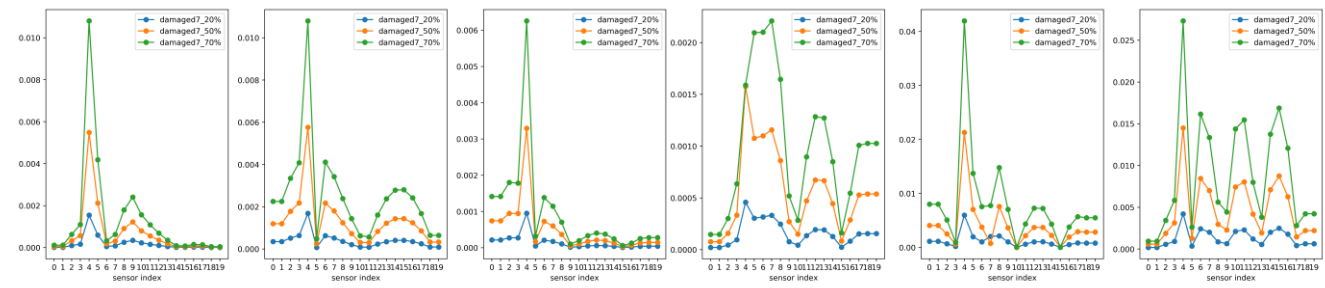
$$\left. \frac{\partial^2 u}{\partial x^2} \right|_i = \frac{u_{i-1} - 2u_i + u_{i+1}}{\text{deltax}^2} + o(\text{deltax})$$

Boundary :

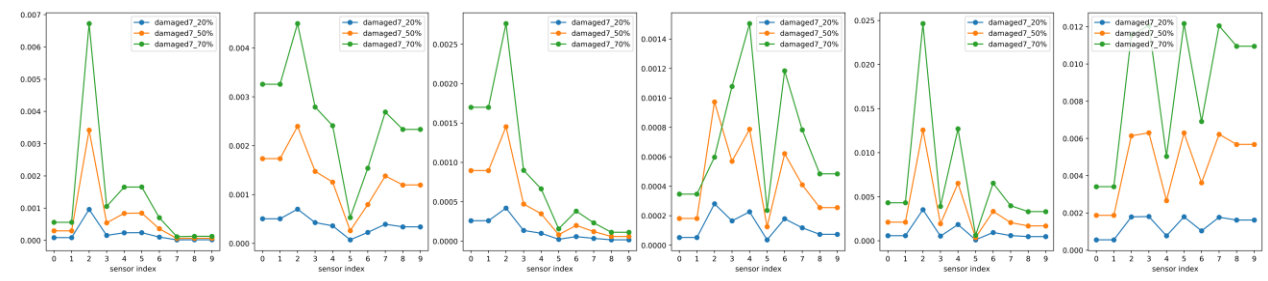
$$\left. \frac{\partial^2 u}{\partial x^2} \right|_{i=0} = \frac{u_0 - 2u_1 + u_2}{\text{deltax}^2} + o(\text{deltax})$$

$$\left. \frac{\partial^2 u}{\partial x^2} \right|_{i=\text{sensor}-1} = \frac{u_{\text{sensor}-3} - 2u_{\text{sensor}-2} + u_{\text{sensor}-1}}{\text{deltax}^2} + o(\text{deltax})$$

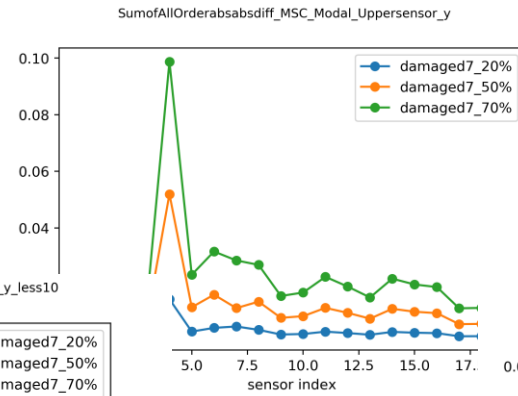
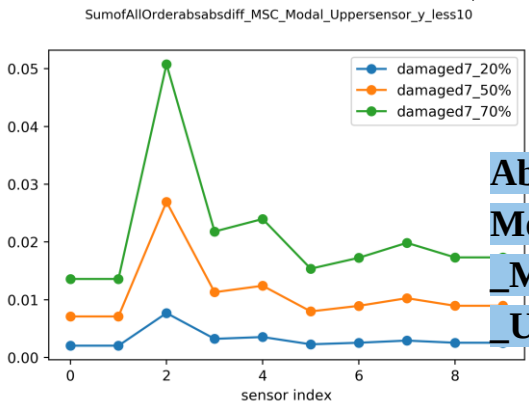
Absabsdiff_ModeShapeCurvature_Modal_eachorder_Uppersensor_y_20



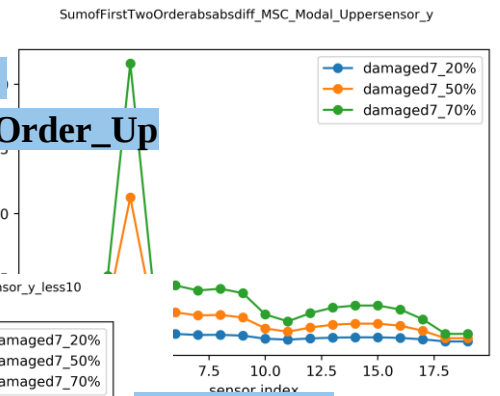
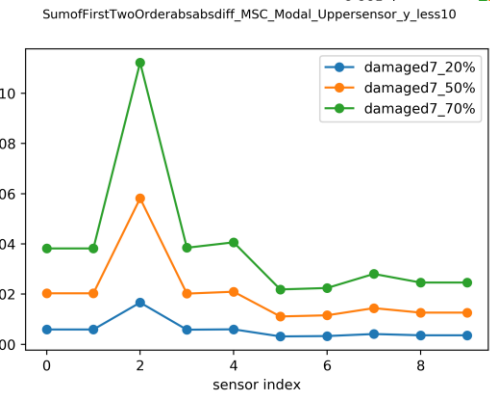
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Absabsdiff_ModeShapeCurvature_Modal_SumAllOrder_Uppersensor_y_20

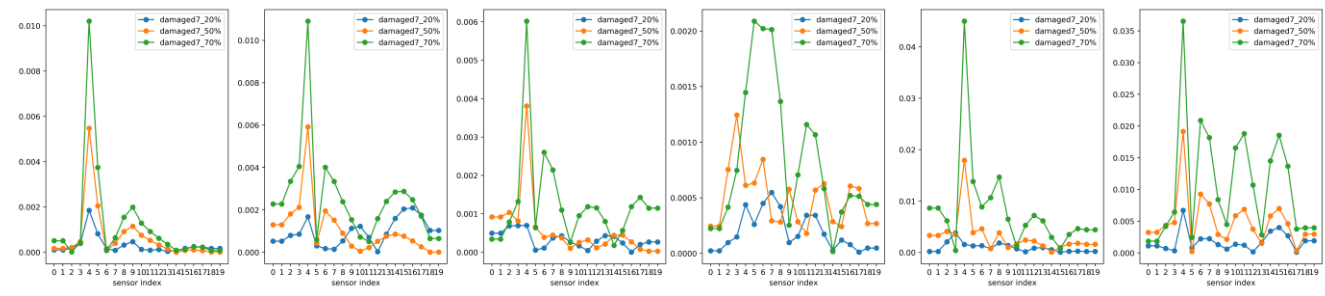


Absabsdiff_ModeShapeCurvature_Modal_SumOfFirst2Order_Uppersensor_y_20

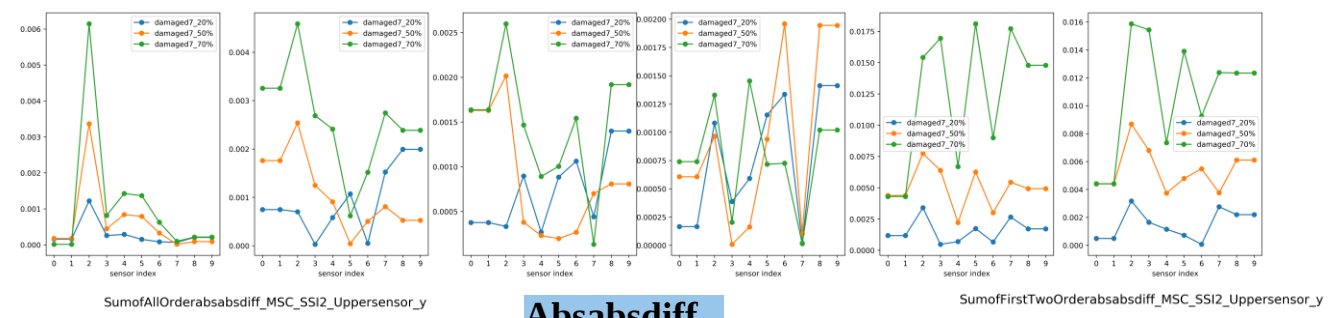


Absabsdiff_ModeShapeCurvature_Modal_SumOfFirst2Order_Uppersensor_y_10

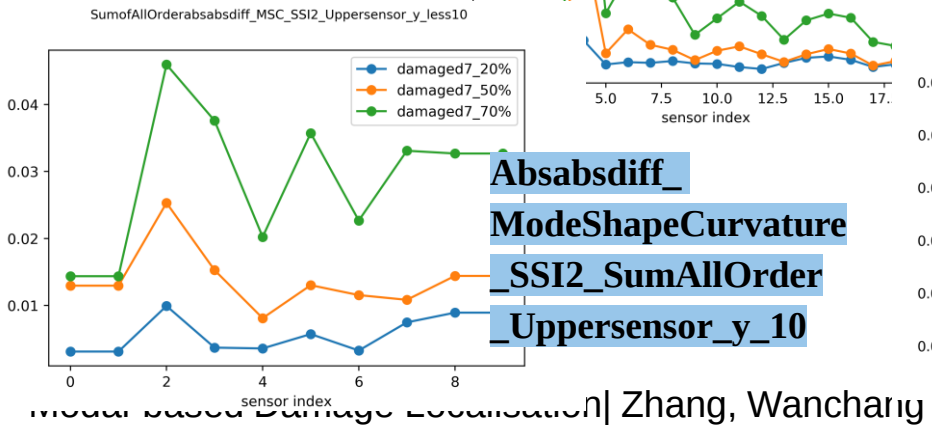
Absabsdiff_ModeShapeCurvature_SSI2_eachorder_Uppersensor_y_20



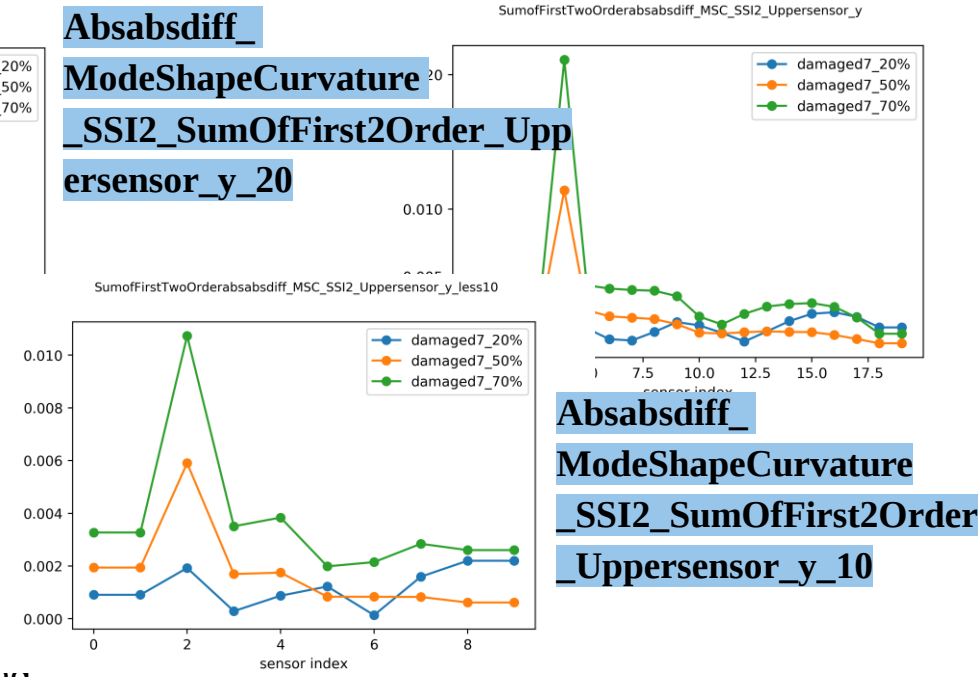
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Absabsdiff_ModeShapeCurvature_SSI2_SumAllOrder_Uppersensor_y_20

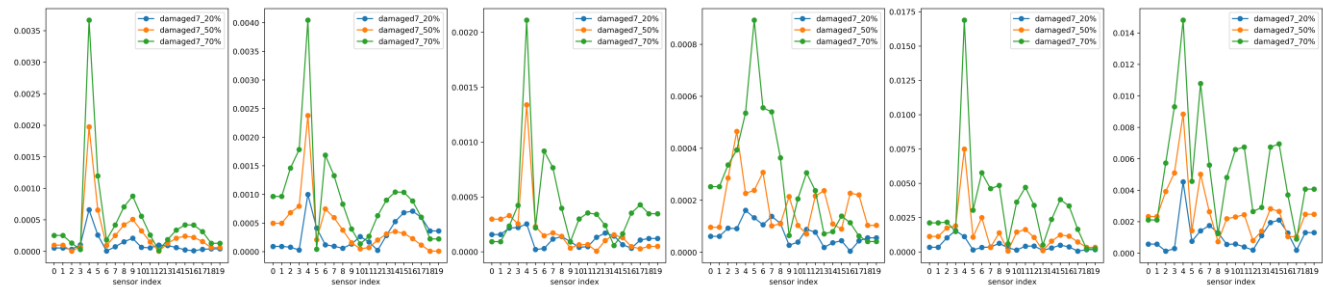


Absabsdiff_ModeShapeCurvature_SSI2_SumAllOrder_Uppersensor_y_10

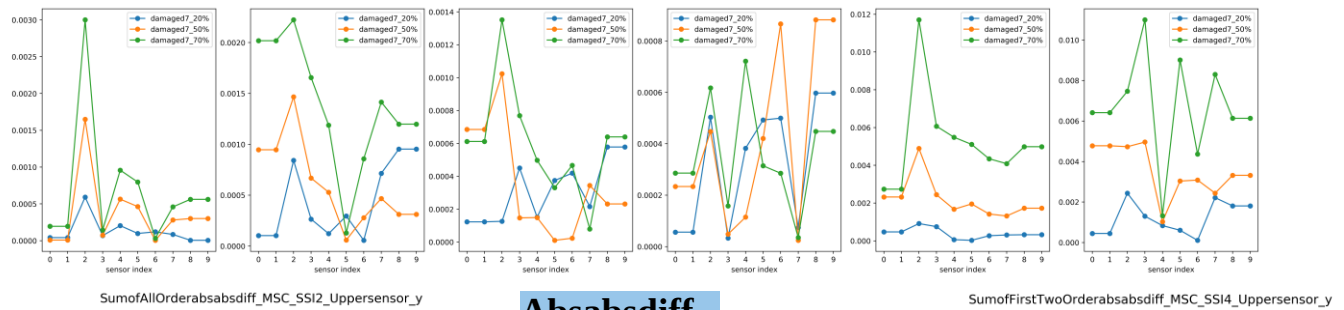


Absabsdiff_ModeShapeCurvature_SSI2_SumOfFirst2Order_Uppersensor_y_10

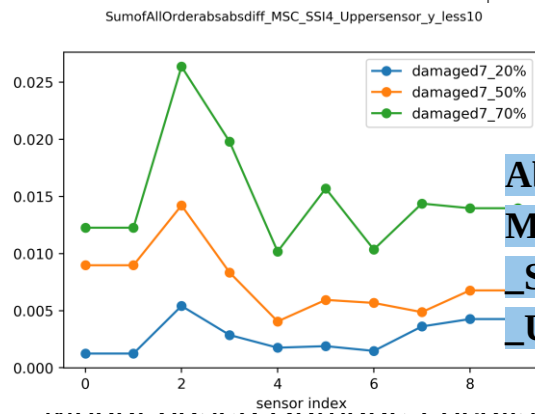
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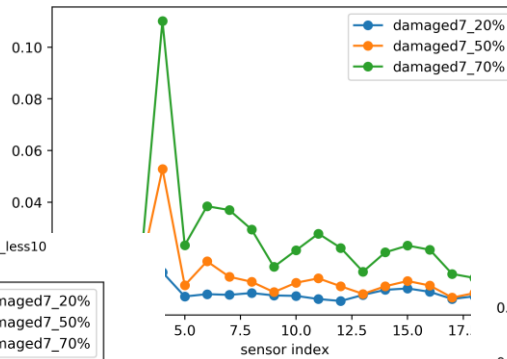
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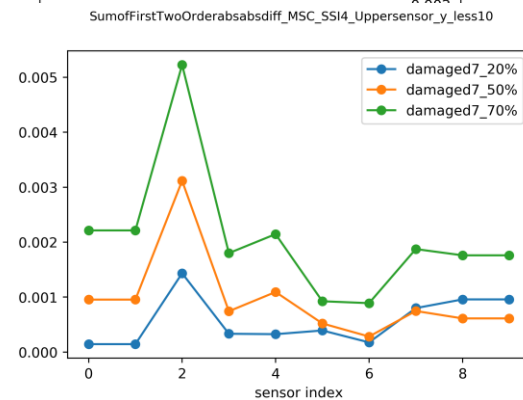
Absabsdiff_ ModeShapeCurvature _SSI4_SumAllOrder _Uppersensor_y_20



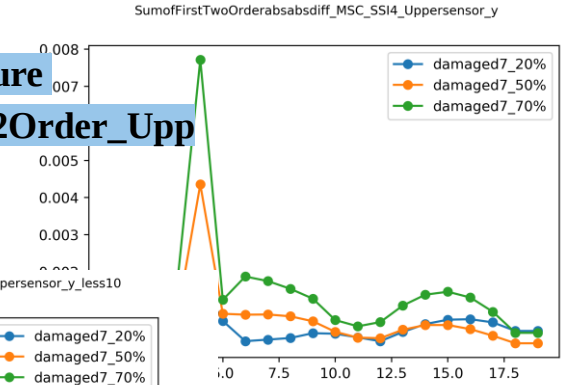
Absabsdiff_ ModeShapeCurvature _SSI4_SumAllOrder _Uppersensor_y_10



Absabsdiff_ ModeShapeCurvature _SSI4_SumOfFirst2Order_Upp ersensor_y_20



Absabsdiff_ ModeShapeCurvature _SSI4_SumOfFirst2Order _Uppersensor_y_10



Part 3 Damage Index derived modal Features

Modal Strain Energy:

The strain energy stored in the spring when the structures deform in one of its mode shapes is:

$$U = \frac{1}{2} k (\Delta x)^2, \Delta x \text{ is the change of length of the springs from its undeformed state}$$

The strain energy U of a Euler-Bernoulli beam of length L is given by $U = \frac{1}{2} \int_0^L EI \left(\frac{\partial^2 w}{\partial x^2} \right)^2 dx$,

w is the transverse displacement of the beam, x is the coordinate along the length of the beam

For a particular mode shape ψ_i , the strain energy associated with the deformation in that mode shape pattern is

$$U_i = \frac{1}{2} \int_0^L EI \left(\frac{\partial^2 \psi_i}{\partial x^2} \right)^2 dx = \frac{1}{2} EI \int_0^L \left(\frac{\partial^2 \psi_i}{\partial x^2} \right)^2 dx$$

Since the beam is subdivided into N divisions as shown in the figure, then the energy associated with each subregion j due to the i th mode is given by

$$U_{ij} = \frac{1}{2} \int_{a_j}^{a_{j+1}} (EI)_j \left(\frac{\partial^2 \psi_i}{\partial x^2} \right)^2 dx = \frac{1}{2} (EI)_j \int_{a_j}^{a_{j+1}} \left(\frac{\partial^2 \psi_i}{\partial x^2} \right)^2 dx$$

The fractional energy is defined as $F_{ij} = \frac{U_{ij}}{U_i}$

Part 3 Damage Index derived modal Features

Modal Strain Energy:

Schematic illustration of a beam's division

0	1	2	...	j	...	N
---	---	---	-----	---	-----	---

Node index 0 1 2 3 ... j j+1 ... N N+1

x position 5dx 15dx 25dx 30dx... a_j a_{j+1} l-15dx l-5dx ($\delta_x=10dx$)

x position 5dx 25dx 45dx 65dx... a_j a_{j+1} l-25dx l-5dx ($\delta_x=20dx$)

Similar quantities can be defined for a damaged structure $F_{ijd} = \frac{U_{ijd}}{U_{id}}$, $\sum_{j=0}^{j=N} F_{ij} = \sum_{j=0}^{j=N} F_{ijd} = 1$

If it is assumed that the damage is primarily located at a single subregion then the fractional energy will remain relatively constant in the undamaged subregions and in the damaged region k $F_{ikd} = F_{ik}$

$$\frac{U_{ikd}}{U_{id}} = \frac{U_{ik}}{U_i} \frac{(EI)_k}{((EI)_d)_k} = \frac{\frac{\int_{a_k}^{a_{k+1}} \left(\frac{\partial^2 \psi_{i,d}}{\partial x^2} \right)^2 dx}{\int_0^l \left(\frac{\partial^2 \psi_{id}}{\partial x^2} \right)^2 dx}}{\frac{\int_{a_k}^{a_{k+1}} \left(\frac{\partial^2 \psi_i}{\partial x^2} \right)^2 dx}{\int_0^l \left(\frac{\partial^2 \psi_i}{\partial x^2} \right)^2 dx}} \equiv \frac{f_{ikd}}{f_{ik}} \quad \text{damage Index } \beta_k = \frac{\sum_{i=1}^m f_{ikd}}{\sum_{i=1}^m f_{ik}}$$

Part 3 Damage Index derived modal Features

Modal Strain Energy:

$$\text{damage Index sum of all order: } \beta_k = \frac{\sum_{i=1}^{i=m} f_{ikd}}{\sum_{i=1}^{i=m} f_{ik}}$$

$$\text{sum of first two order } \beta_{2k} = \frac{\sum_{i=1}^{i=2} f_{ikd}}{\sum_{i=1}^{i=2} f_{ik}}$$

Fractional energy $f_{\text{modal}}(f_{\text{SSI}})$:

beta:

Uppersensor_y_20 # Uppersensor_y_10

beta2:

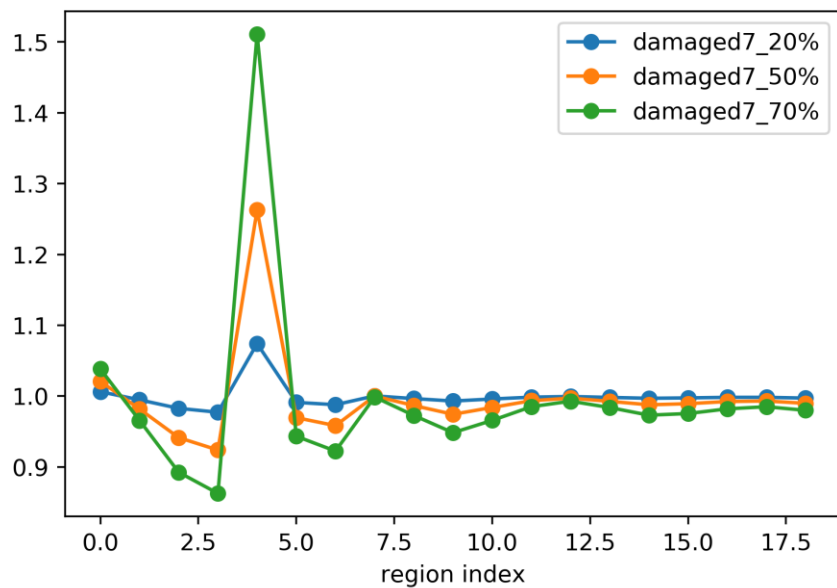
#Uppersensor_y_20 #Uppersensor_y_10

The cubic spline interpolation is done for the modes in python:

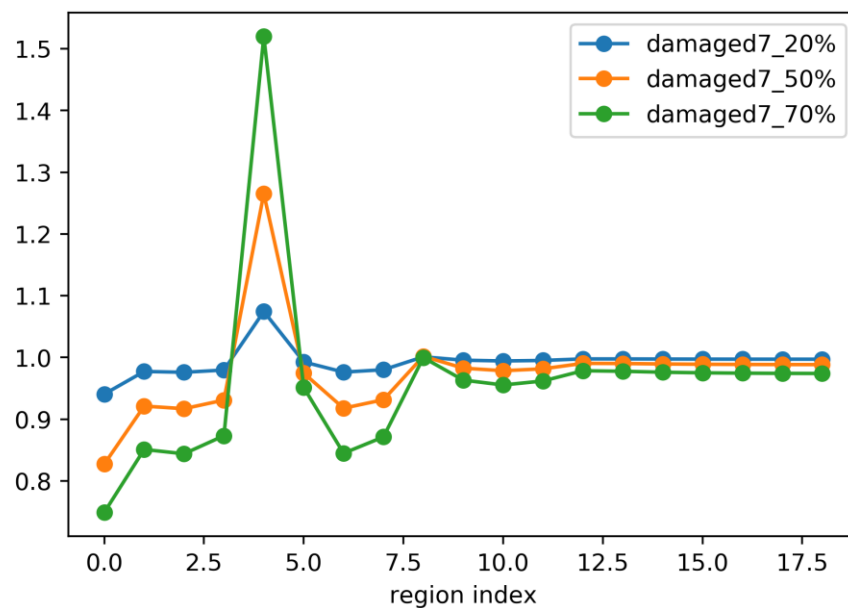
The deviation is analytically

The integration is obtained by the summation

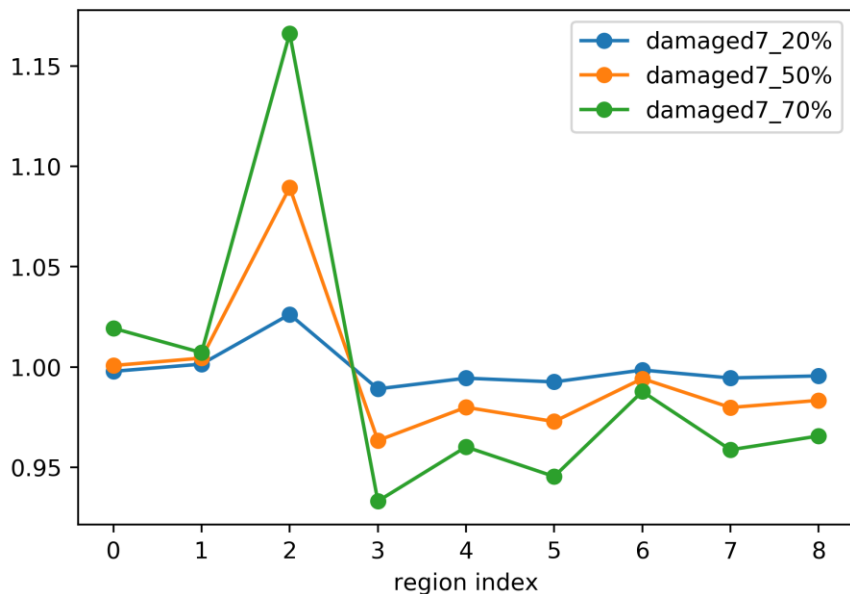
ModalStrainEnergybeta_Modal_Uppersensor_y



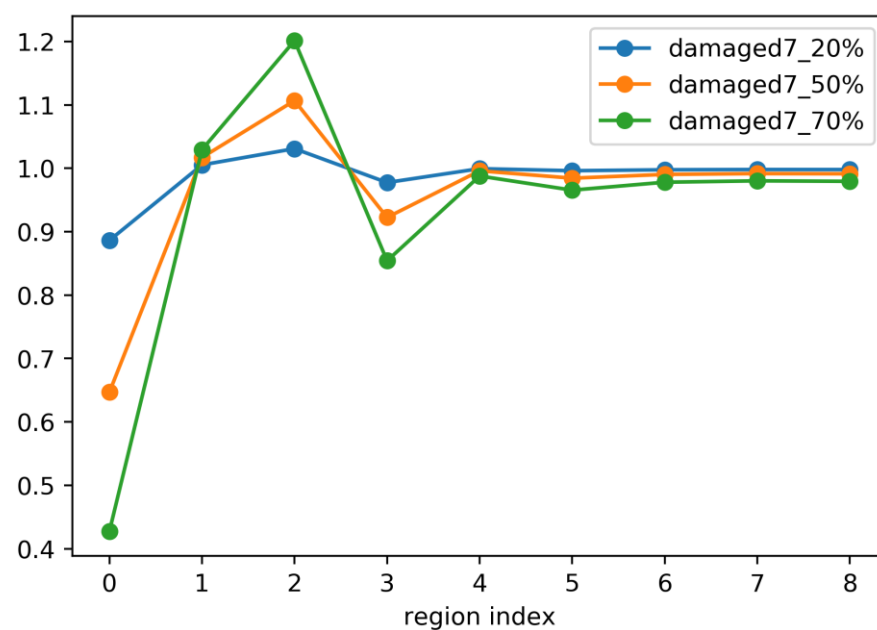
ModalStrainEnergybeta2_Modal_Uppersensor_y



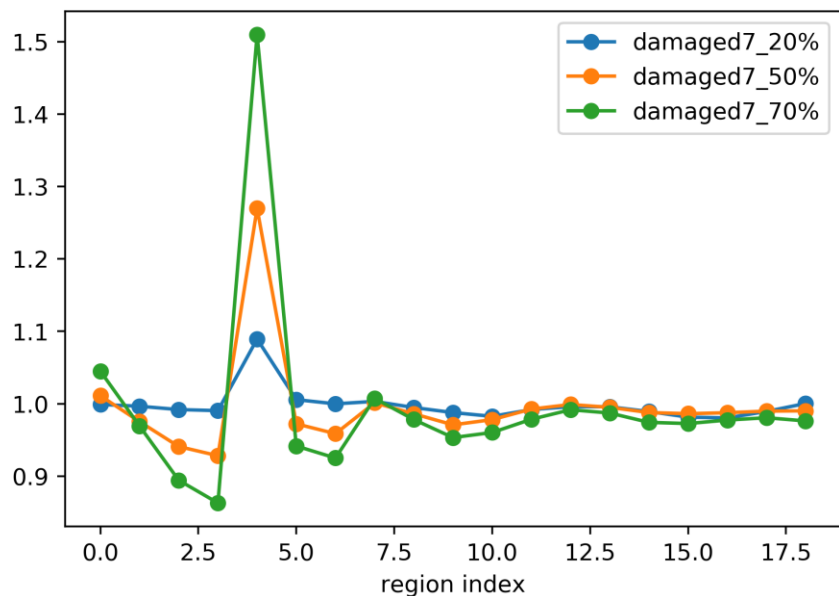
ModalStrainEnergybeta_Modal_Uppersensor_y_less10



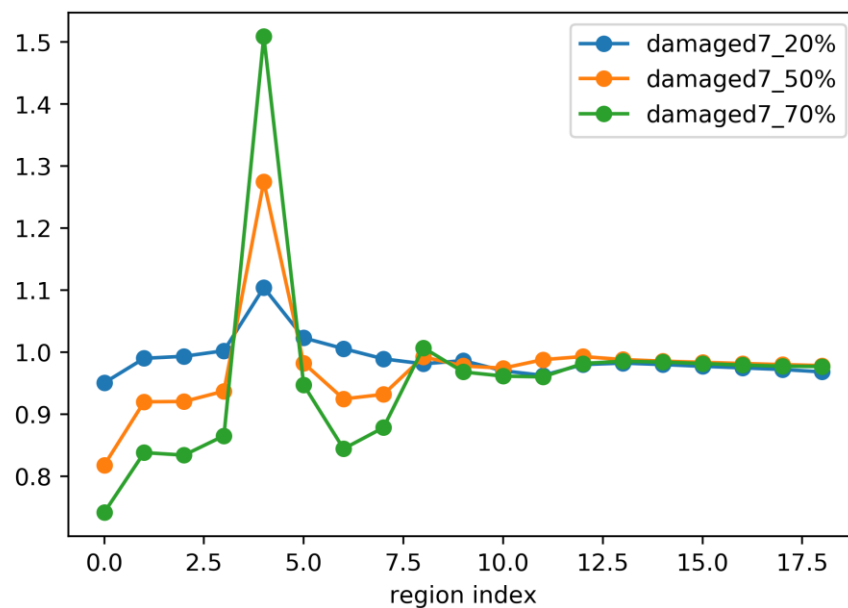
ModalStrainEnergybeta2_Modal_Uppersensor_y_less10



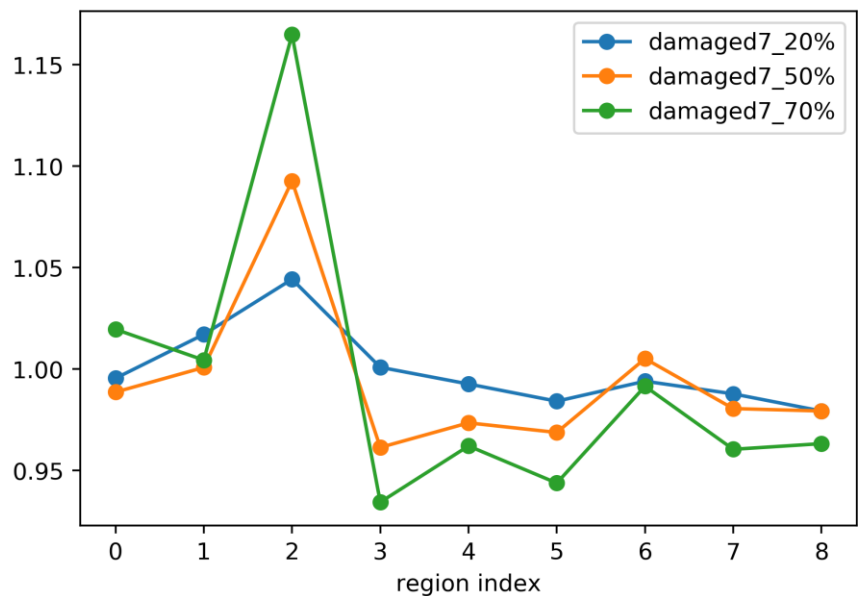
ModalStrainEnergybeta_SSI2_Uppersensor_y



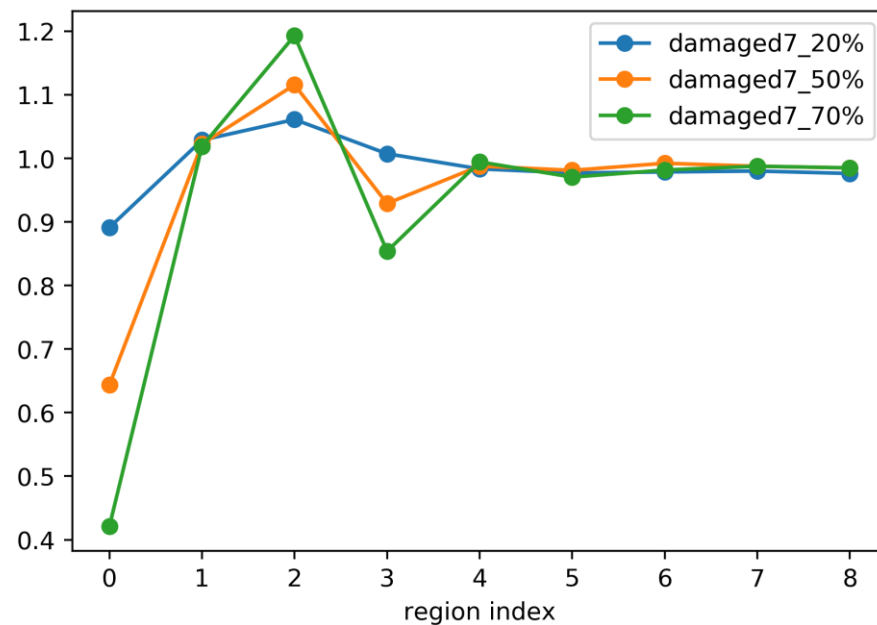
ModalStrainEnergybeta2_SSI2_Uppersensor_y



ModalStrainEnergybeta_SSI2_Uppersensor_y_less10



ModalStrainEnergybeta2_SSI2_Uppersensor_y_less10



Part 3 Damage Index derived modal Features

Flexibility Matrix:

$$[f] = [k][y]$$

$$[y] = [k]^{-1}[f] = [G][f]$$

$[f]$ is the vector of static loads applied to the structure and

$[y]$ is a vector corresponding to the deformation

For an undamaged structure with m **mass-normalised** modal vectors identified from experimental data obtained at n degrees of freedom, the $n \times n$ flexibility matrix $[G]$ can be derived from the modal data as follows¹:

$$[G] \approx [\Phi][\Lambda][\Phi]^T \approx \sum_{i=1}^{i=m} \frac{1}{\omega_i^2} [\psi]_i [\psi]_i^T$$

$[\Phi]$ = the mode shape matrix = $[[\psi]_1, [\psi]_2, \dots, [\psi]_m]$,

$[\psi]_i$ = the i^{th} mass normalised mode shape,

$[\Lambda]$ = the modal stiffness matrix = $\text{diag}(\omega_i^2)$,

ω_i = the i^{th} modal frequency

Part 3 Damage Index derived modal Features

Flexibility Matrix:

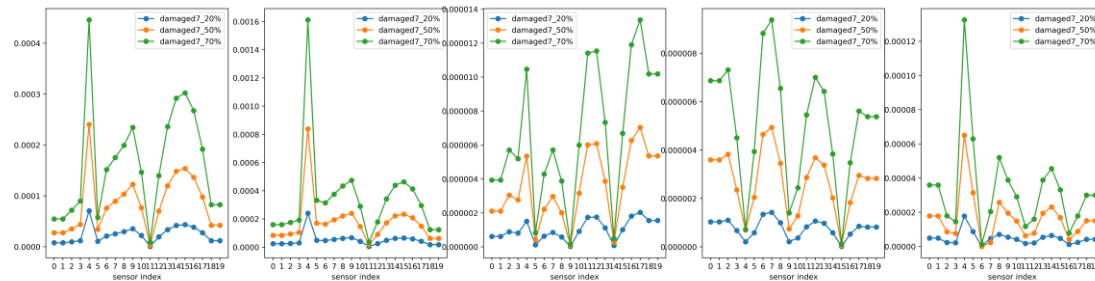
$$[G] \approx [\Phi][\Lambda][\Phi]^T \approx \sum_{i=1}^m \frac{1}{\omega_i^2} [\psi]_i [\psi]_i^T$$

For each order define:

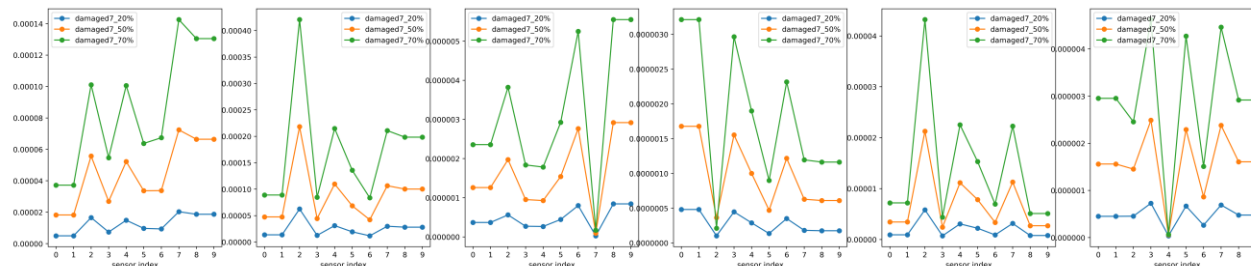
$$[g] \approx \frac{1}{\omega_i^2} [\psi]_i [\psi]_i^T$$

	1 st mode	2 nd mode	...	m th mode	
$\begin{bmatrix} [g_{undamaged}] \\ [g_{damaged}] \end{bmatrix}$	$\begin{bmatrix} a_{11} & \cdots & a_{1n} \\ \vdots & \ddots & \vdots \\ a_{n1} & \cdots & a_{nn} \end{bmatrix}_{n \times n}$	$\begin{bmatrix} a_{11} & \cdots & a_{1n} \\ \vdots & \ddots & \vdots \\ a_{n1} & \cdots & a_{nn} \end{bmatrix}_{n \times n}$	...	$\begin{bmatrix} a_{11} & \cdots & a_{1n} \\ \vdots & \ddots & \vdots \\ a_{n1} & \cdots & a_{nn} \end{bmatrix}_{n \times n}$	
$\begin{bmatrix} \mathbf{v}_{undamaged} \\ \mathbf{v}_{damaged} \end{bmatrix}$	$\begin{bmatrix} a_{11} + \cdots + a_{1n} \\ \vdots \\ a_{n1} + \cdots + a_{nn} \end{bmatrix}_{n \times 1}$	$\begin{bmatrix} a_{11} + \cdots + a_{1n} \\ \vdots \\ a_{n1} + \cdots + a_{nn} \end{bmatrix}_{n \times 1}$	...	$\begin{bmatrix} a_{11} + \cdots + a_{1n} \\ \vdots \\ a_{n1} + \cdots + a_{nn} \end{bmatrix}_{n \times 1}$	
$\begin{bmatrix} \mathbf{v}_{curvature_undamaged} \\ \mathbf{v}_{curvature_damaged} \end{bmatrix}$	$\begin{bmatrix} c_1 \\ \vdots \\ c_n \end{bmatrix}_{n \times 1}$	$\begin{bmatrix} c_1 \\ \vdots \\ c_n \end{bmatrix}_{n \times 1}$	...	$\begin{bmatrix} c_1 \\ \vdots \\ c_n \end{bmatrix}_{n \times 1}$	$\left. \vphantom{\begin{bmatrix} c_1 \\ \vdots \\ c_n \end{bmatrix}} \right\} \text{DamageIndex:Diff_vc}$

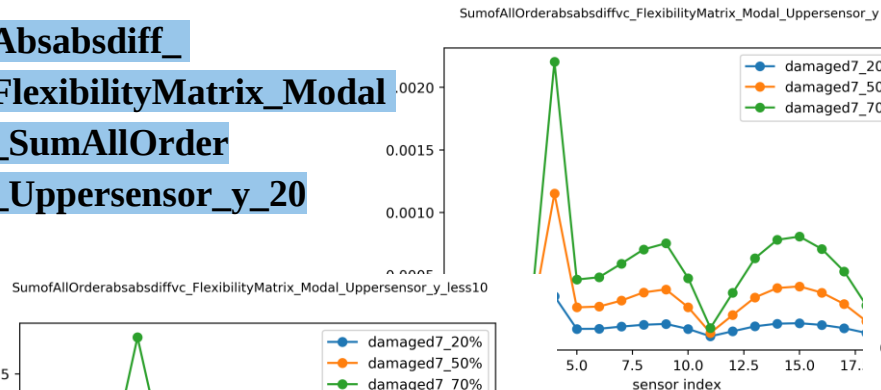
Absabsdiff_FlexibilityMatrix_Modal_eachorder_Uppersensor_y_20



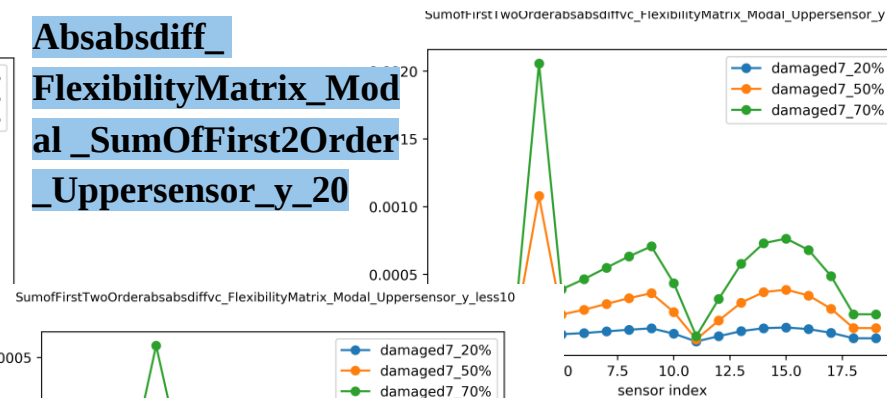
Absabsdiff_FlexibilityMatrix_Modal_eachorder_Uppersensor_y_10



Absabsdiff_FlexibilityMatrix_Modal_SumAllOrder_Uppersensor_y_20



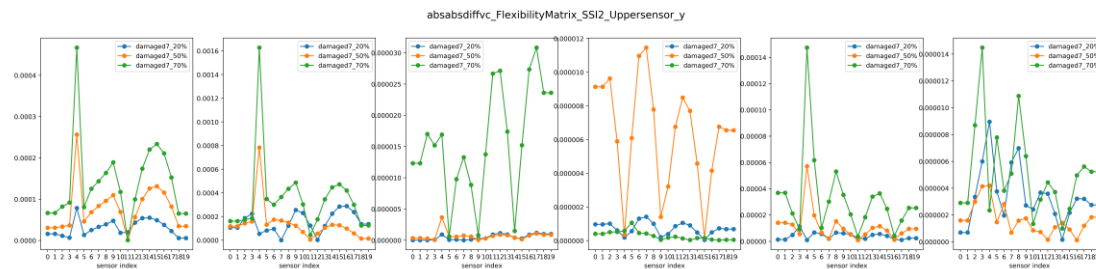
Absabsdiff_FlexibilityMatrix_Modal_SumOfFirst2Order_Uppersensor_y_20



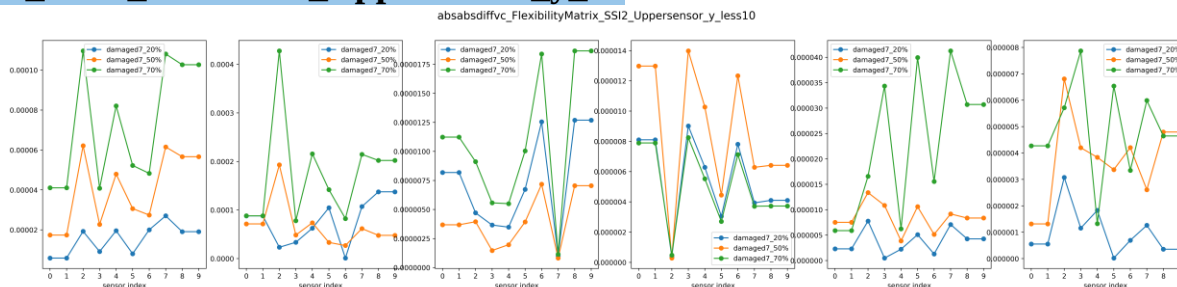
Absabsdiff_FlexibilityMatrix_Modal_SumAllOrder_Uppersensor_y_10

Absabsdiff_FlexibilityMatrix_Modal_SumOfFirst2Order_Uppersensor_y_10

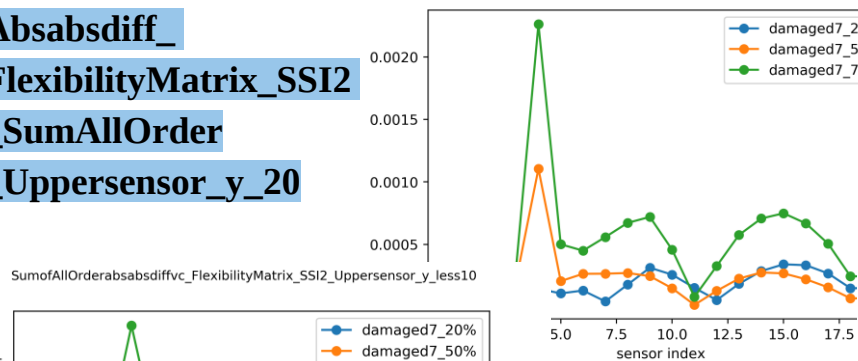
Absabsdiff_FlexibilityMatrix_SSI2_eachorder_Uppersensor_y_20



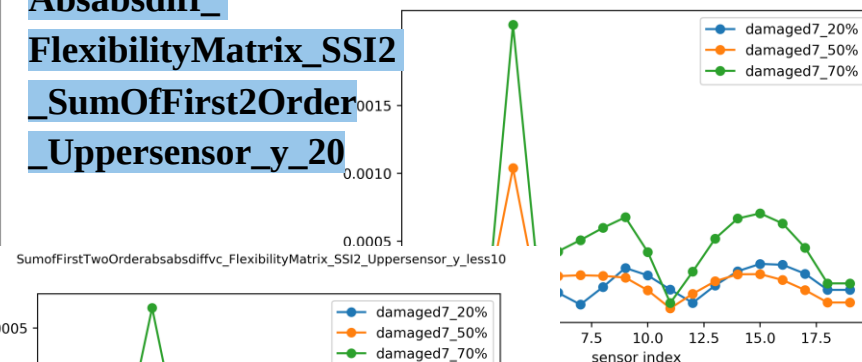
Absabsdiff_FlexibilityMatrix_SSI2_eachorder_Uppersensor_y_10



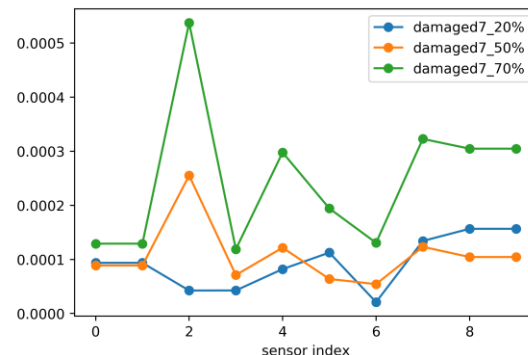
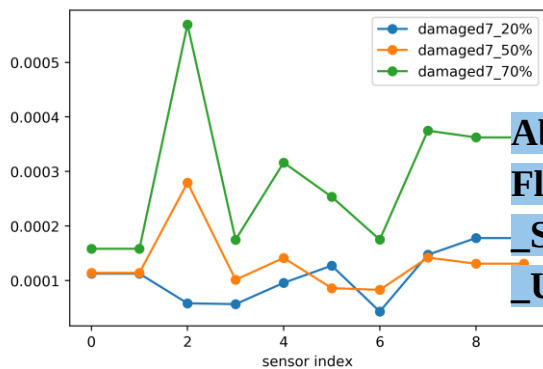
Absabsdiff_FlexibilityMatrix_SSI2_SumAllOrder_Uppersensor_y_20



Absabsdiff_FlexibilityMatrix_SSI2_SumOfFirst2Order_Uppersensor_y_20



Absabsdiff_FlexibilityMatrix_SSI2_SumAllOrder_Uppersensor_y_10



Absabsdiff_FlexibilityMatrix_SSI2_SumOfFirst2Order_Uppersensor_y_10

Part 4 Summary

Mode Shape Curvature:

- + easy to operate, informative result**
- + only needs consistent normalized mode shape**
- higher order not very informative**

Modal Strain Energy:

- + only needs consistent normalized mode shape**
- higher order not very informative**

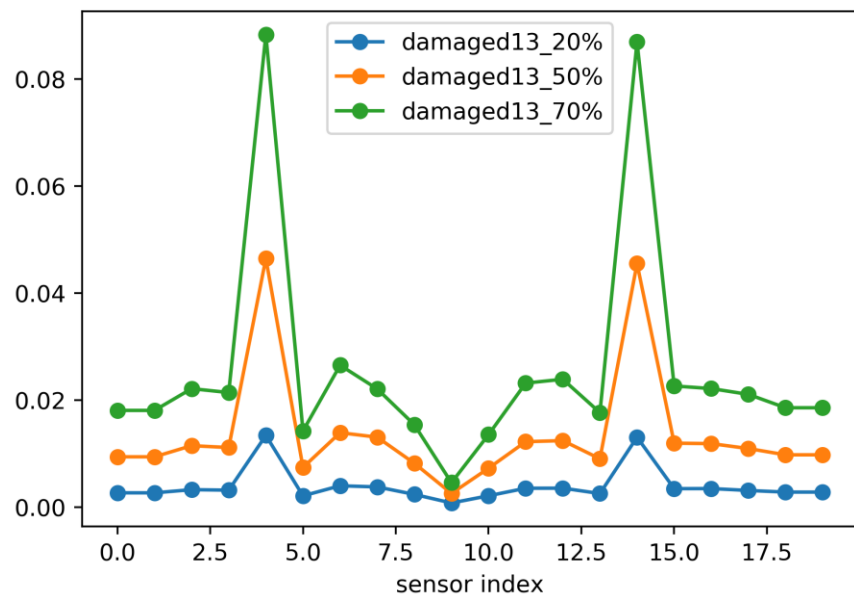
Flexibility Matrix:

- + Higher order mode should be informative**
- need mass normalized mode shape which is not easy to obtain**

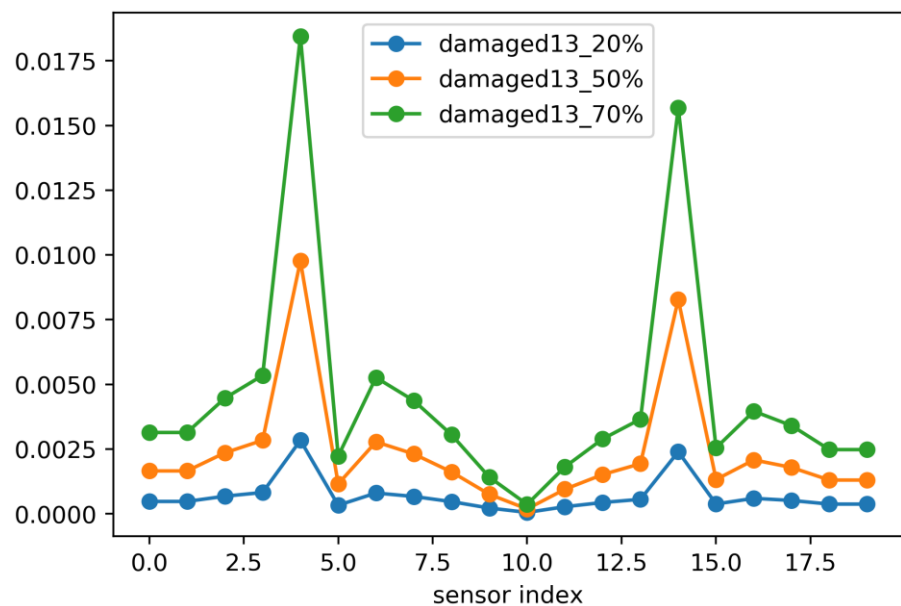
- **One step further**

- Simultaneously apply damaged 7 and damaged 12 (we call it damage 13)
- Mode Shape Curvature
- Modal Strain energy
- Flexibility matrix

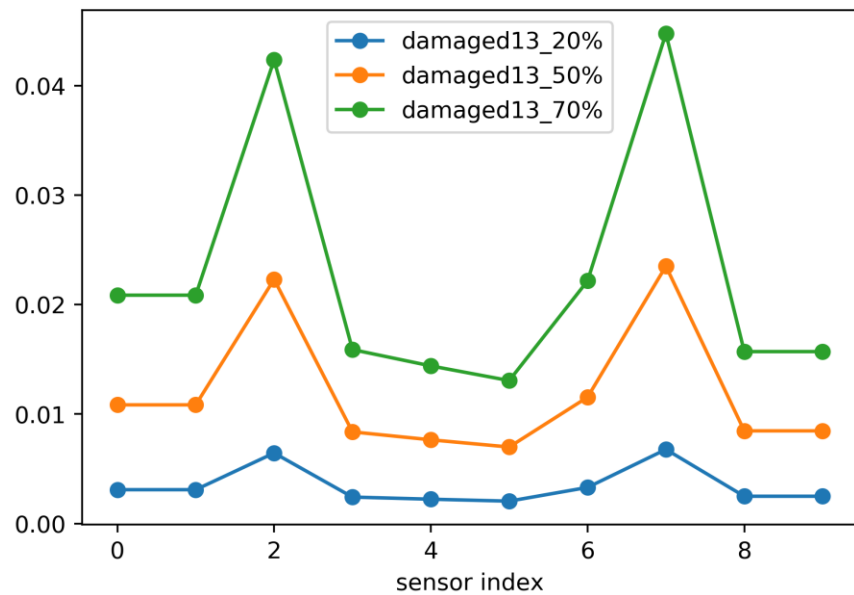
SumofAllOrderabsabsdiff_MSC_Modal_Uppersensor_y



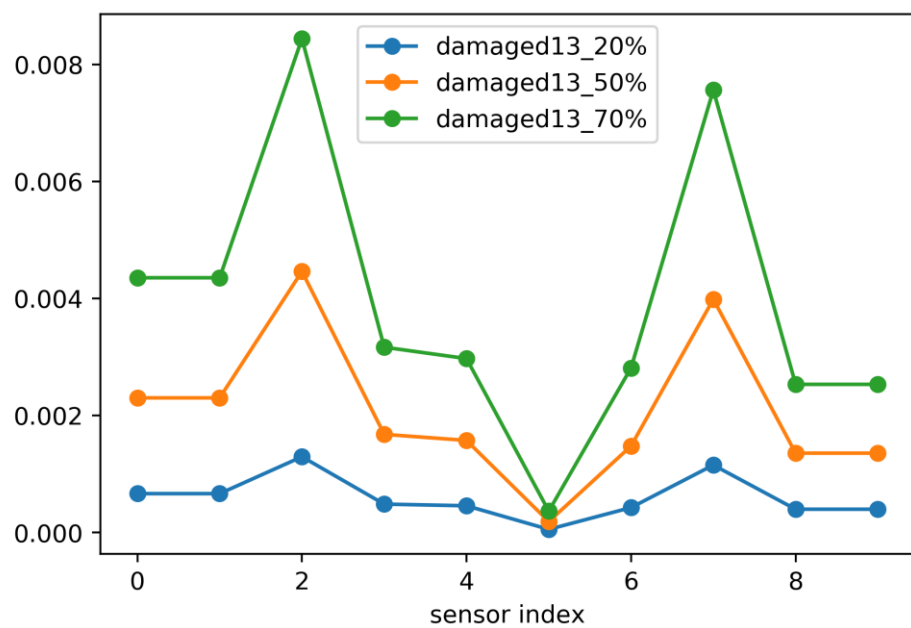
SumofFirstTwoOrderabsabsdiff_MSC_Modal_Uppersensor_y



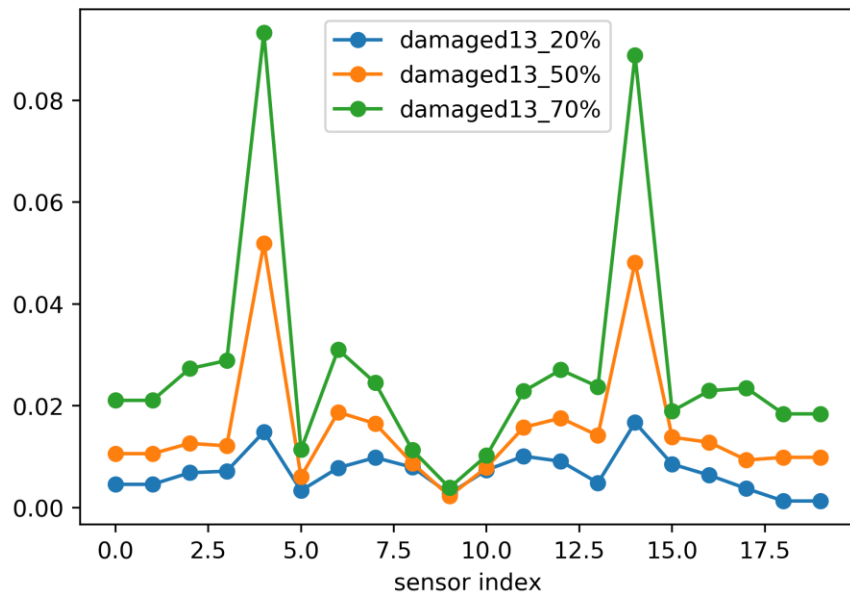
SumofAllOrderabsabsdiff_MSC_Modal_Uppersensor_y_less10



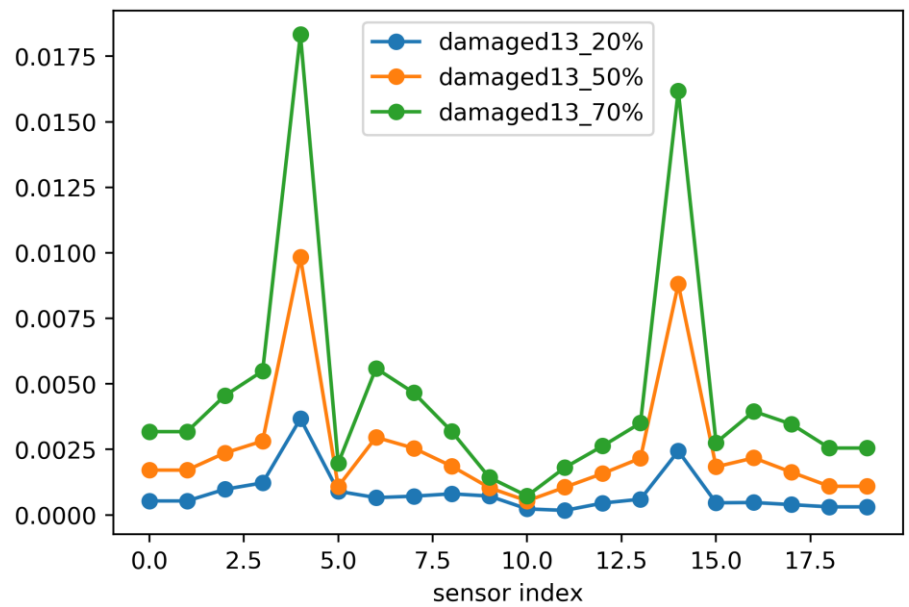
SumofFirstTwoOrderabsabsdiff_MSC_Modal_Uppersensor_y_less10



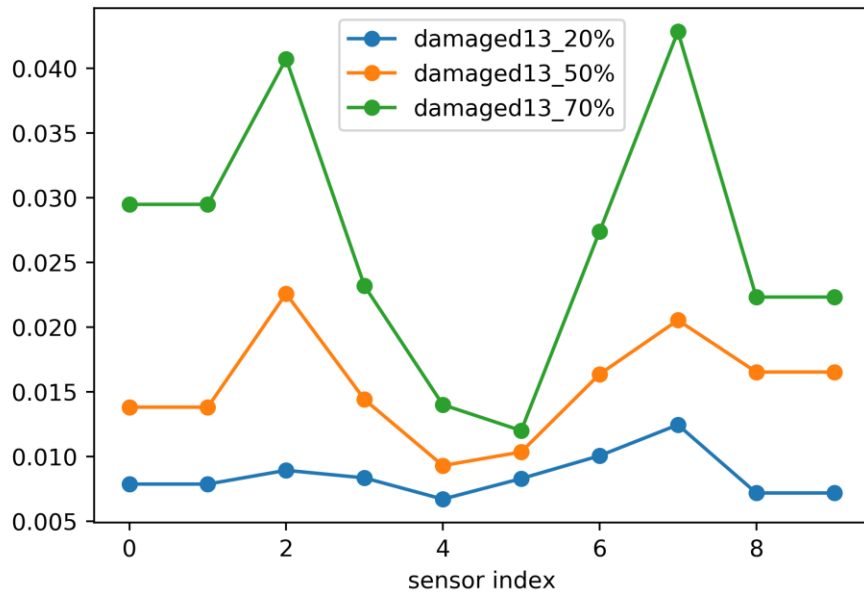
SumofAllOrderabsabsdiff_MSC_SSI2_Uppersensor_y



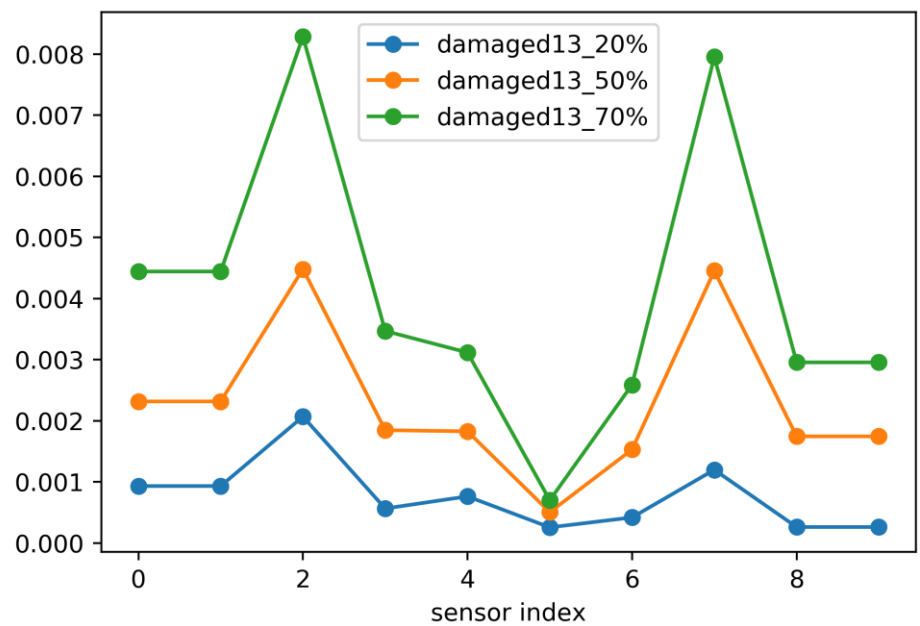
SumofFirstTwoOrderabsabsdiff_MSC_SSI2_Uppersensor_y



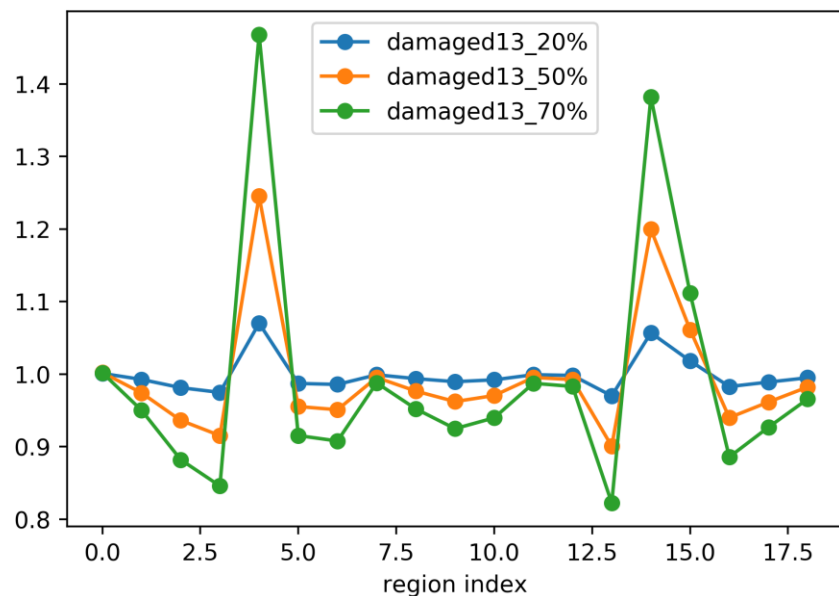
SumofAllOrderabsabsdiff_MSC_SSI2_Uppersensor_y_less10



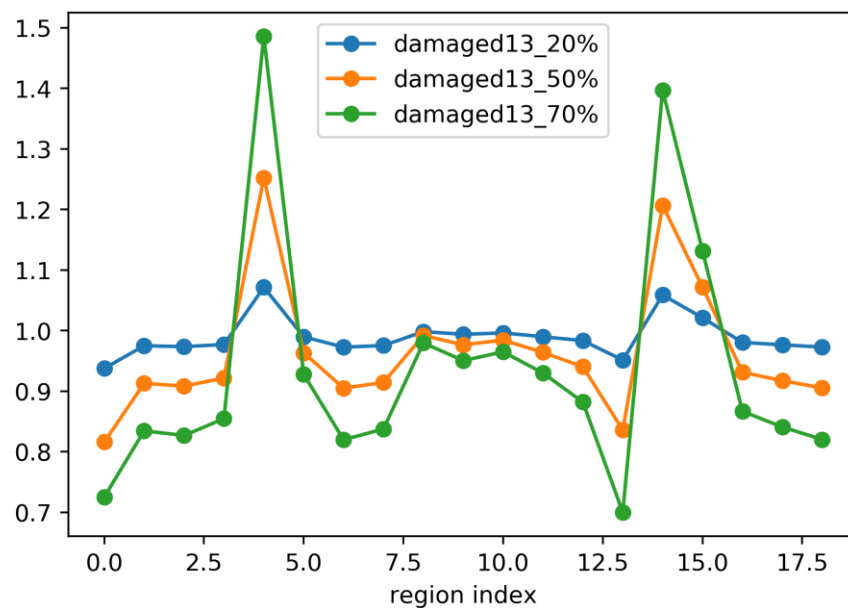
SumofFirstTwoOrderabsabsdiff_MSC_SSI2_Uppersensor_y_less10



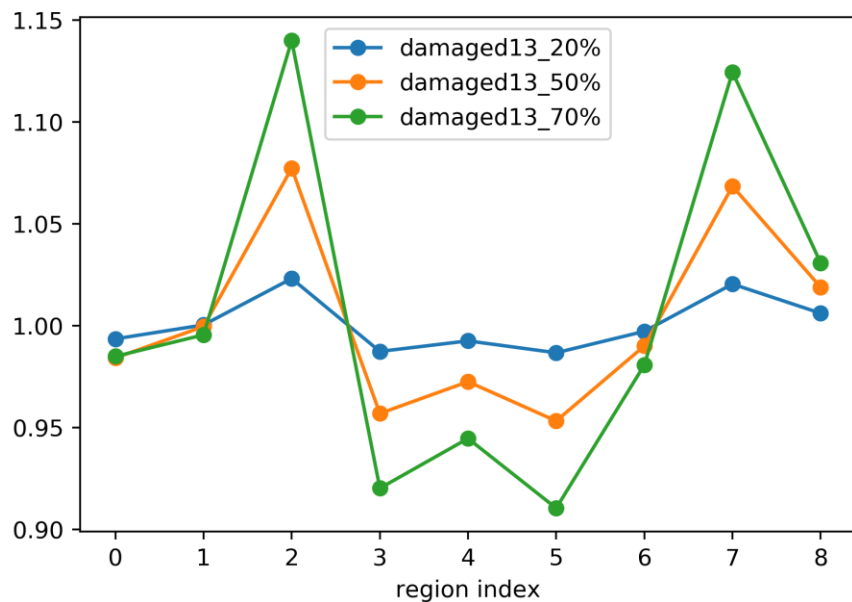
ModalStrainEnergybeta_Modal_Uppersensor_y



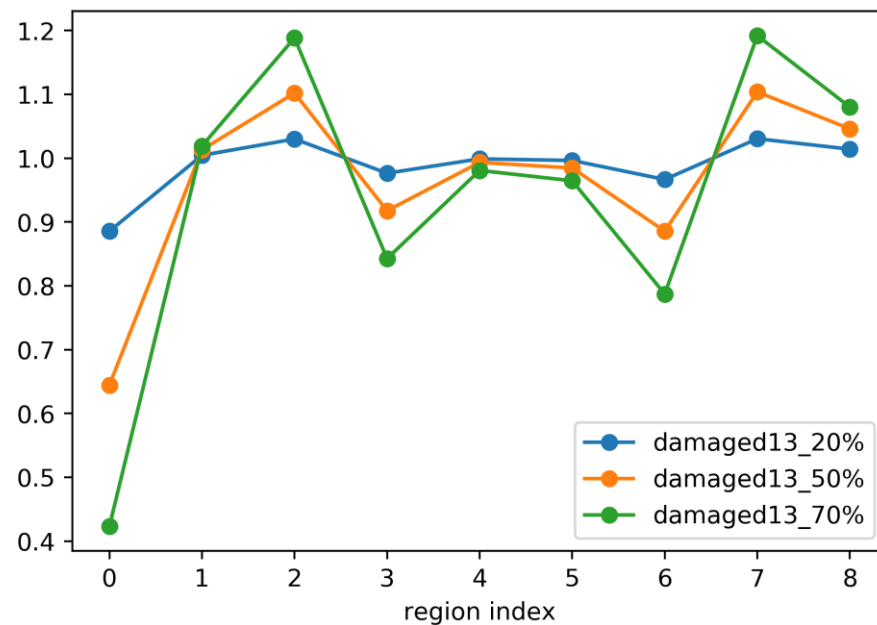
ModalStrainEnergybeta2_Modal_Uppersensor_y



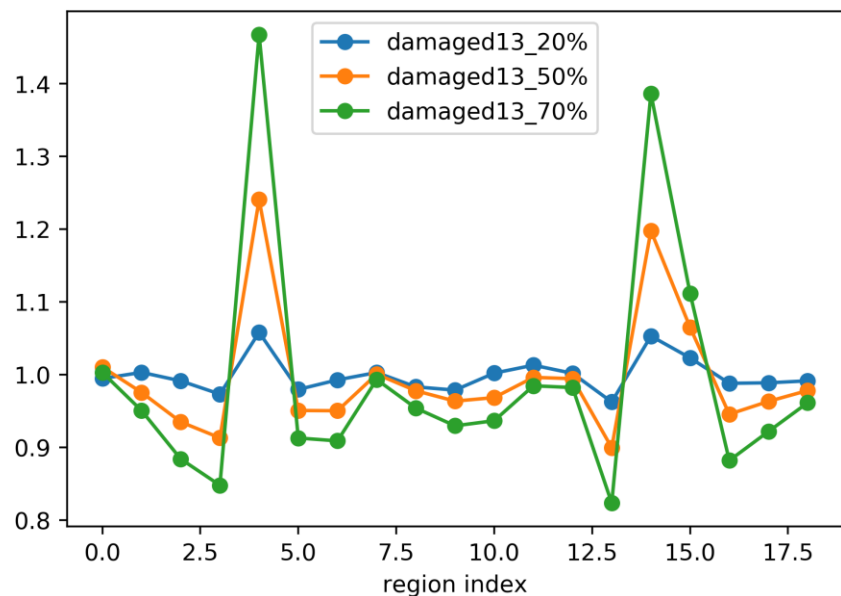
ModalStrainEnergybeta_Modal_Uppersensor_y_less10



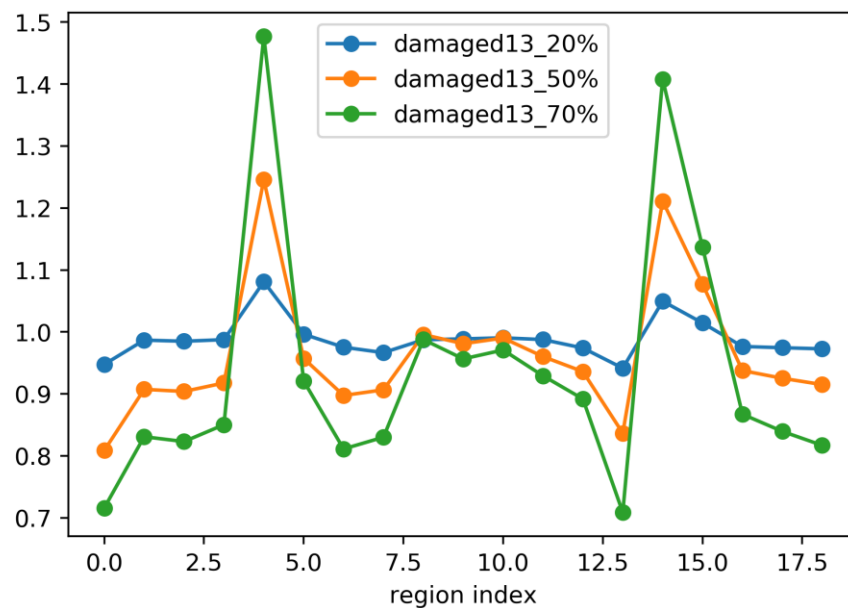
ModalStrainEnergybeta2_Modal_Uppersensor_y_less10



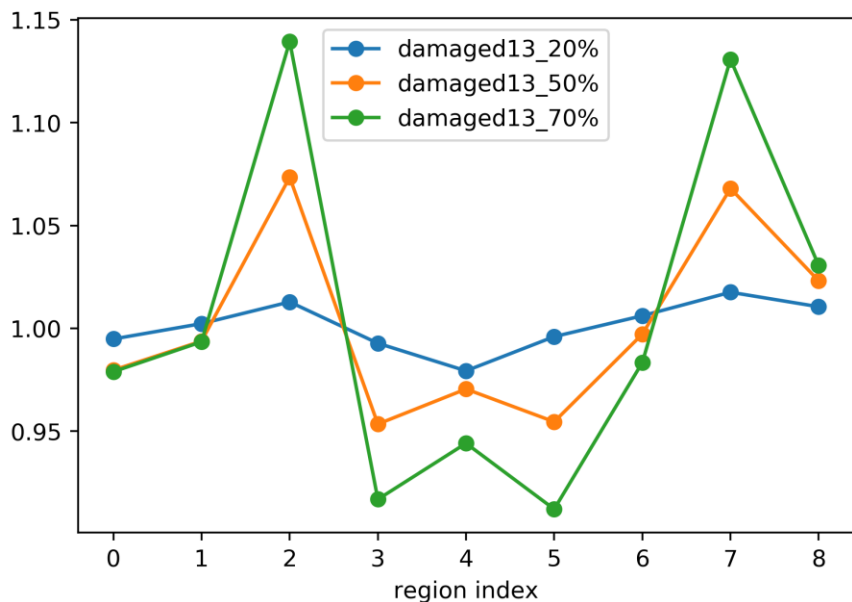
ModalStrainEnergybeta_SSI2_Uppersensor_y



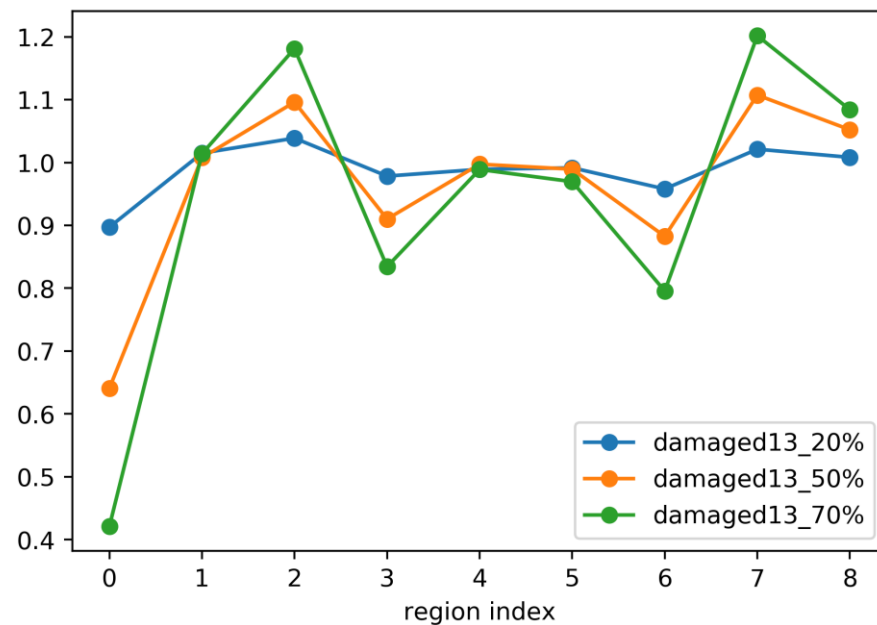
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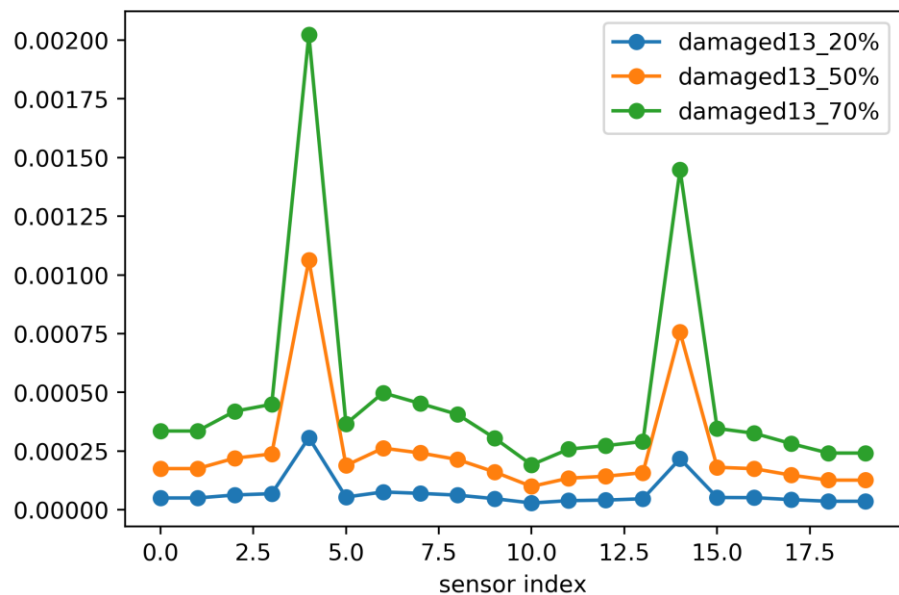
ModalStrainEnergybeta_SSI2_Uppersensor_y_less10



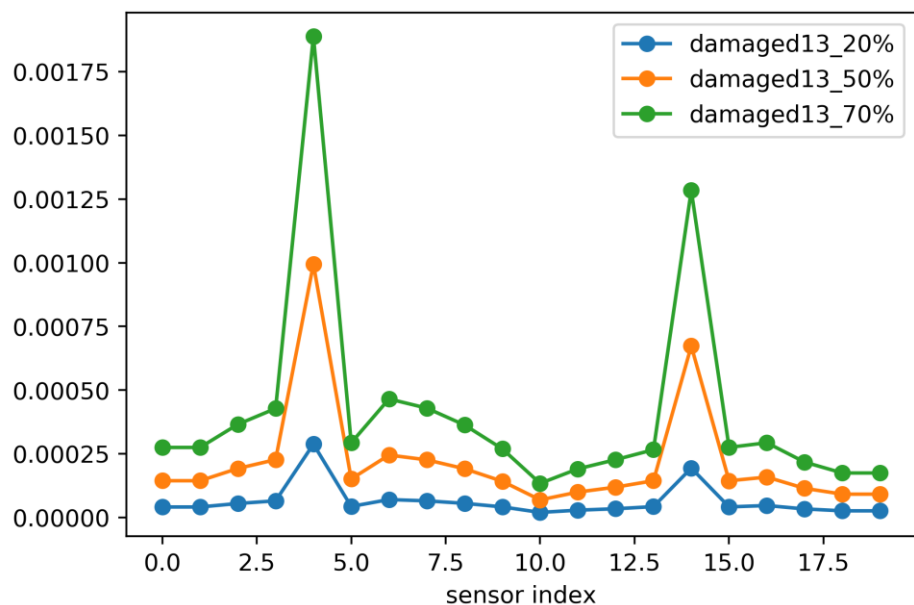
ModalStrainEnergybeta2_SSI2_Uppersensor_y_less10



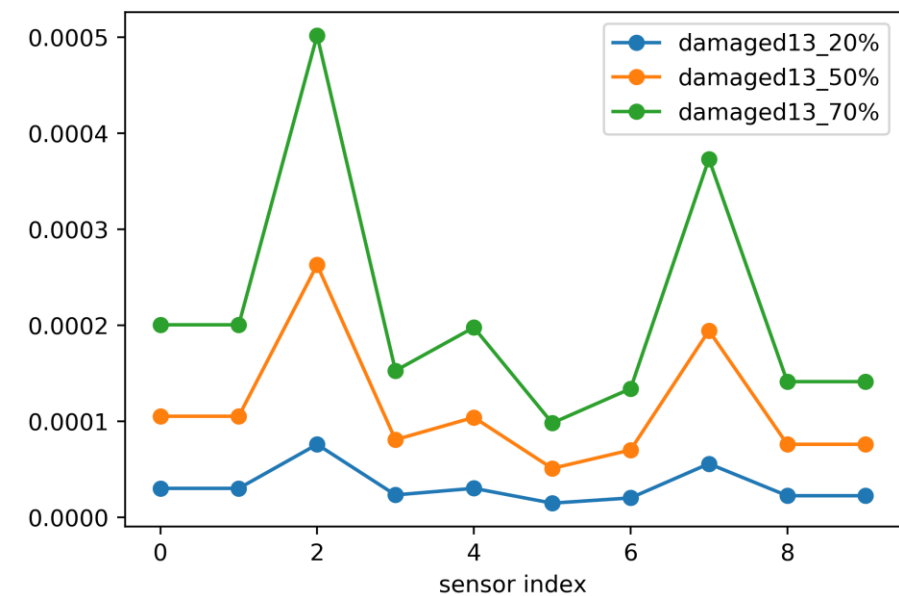
SumofAllOrderabsabsdiffvc_FlexibilityMatrix_Modal_Uppersensor_y



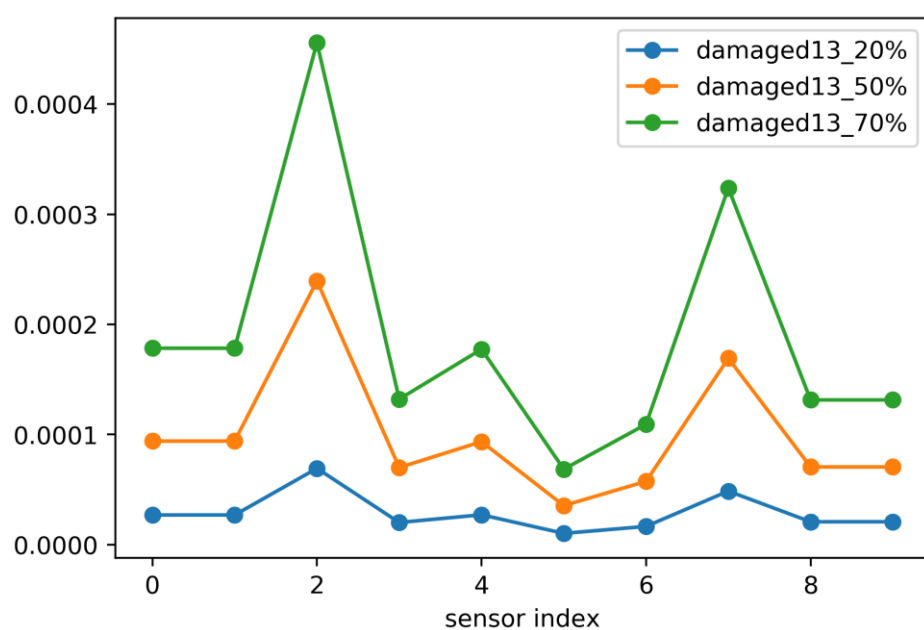
SumofFirstTwoOrderabsabsdiffvc_FlexibilityMatrix_Modal_Uppersensor_y



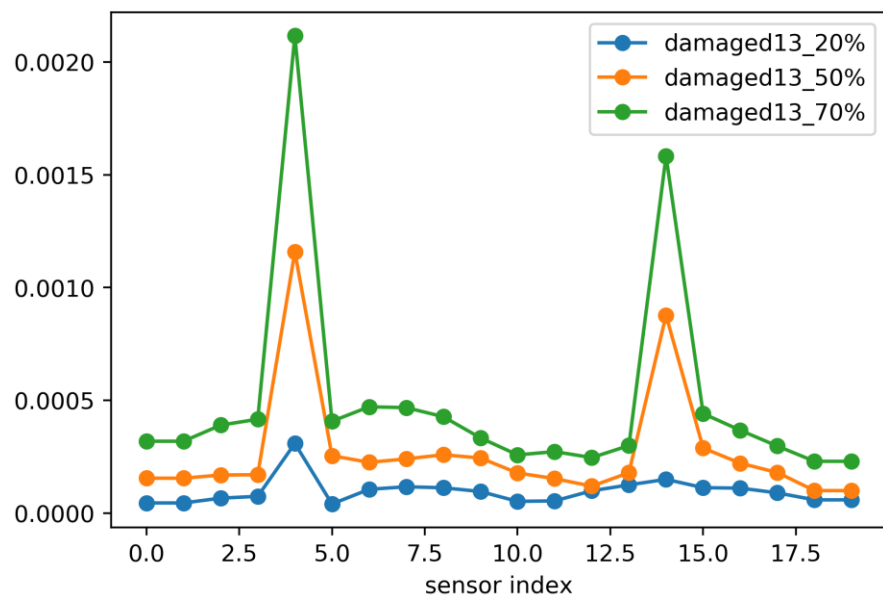
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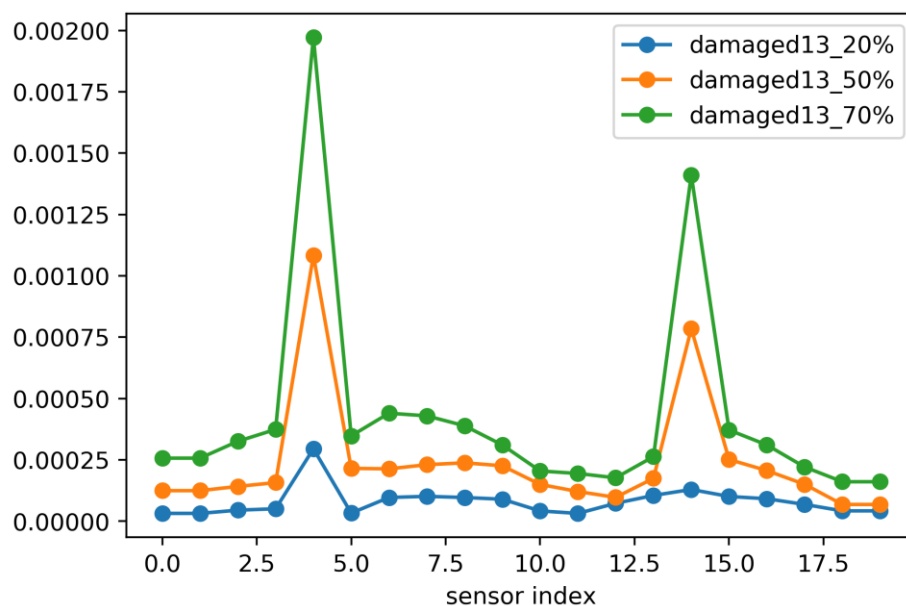
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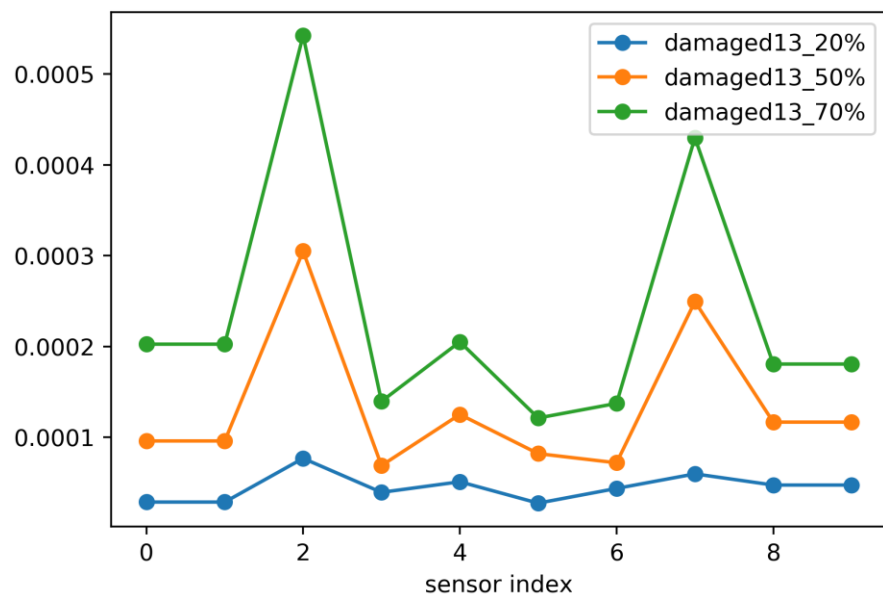
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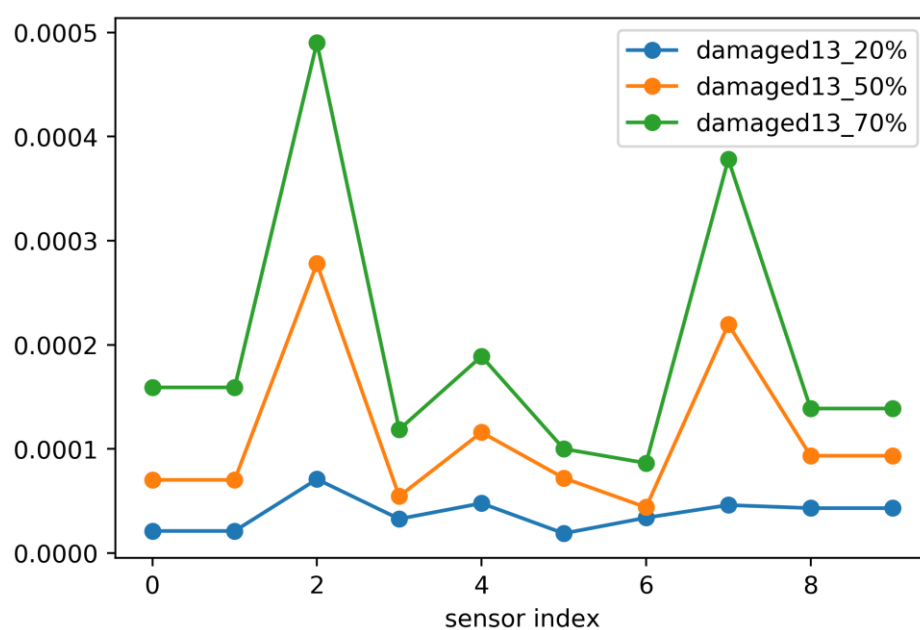
SumofFirstTwoOrderabsabsdiffvc_FlexibilityMatrix_SSI2_Uppersensor_y



SumofAllOrderabsabsdiffvc_FlexibilityMatrix_SSI2_Uppersensor_y_less10



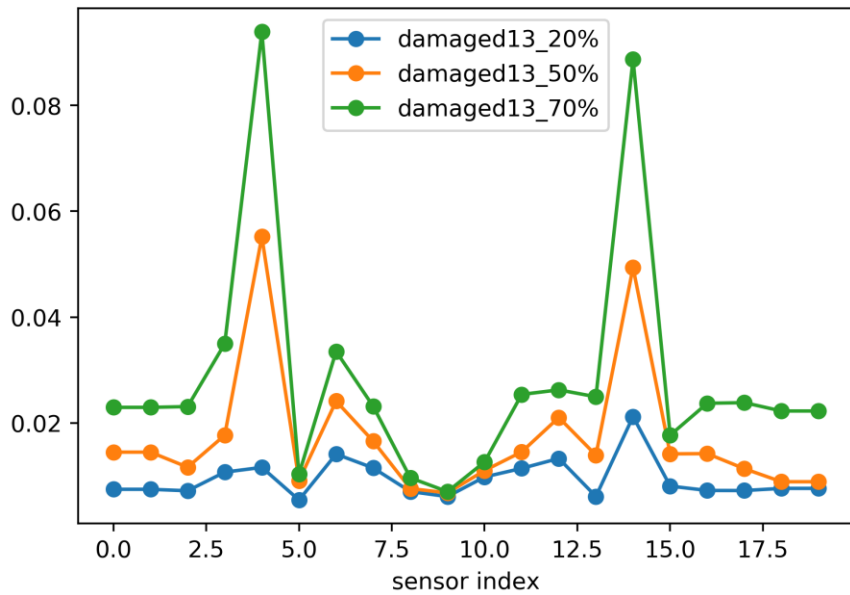
SumofFirstTwoOrderabsabsdiffvc_FlexibilityMatrix_SSI2_Uppersensor_y_less10



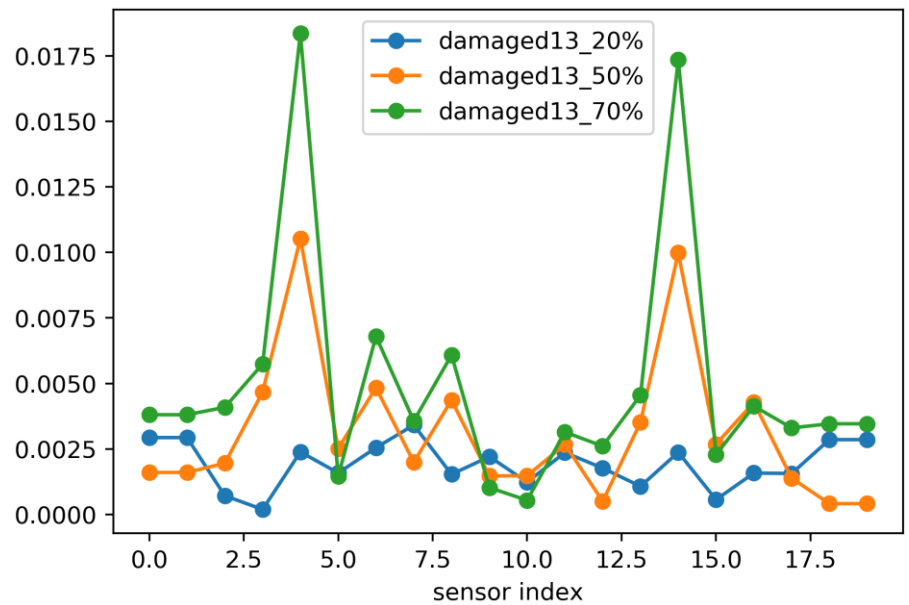
- **Two steps further**

- Simultaneously apply damaged 7 and damaged 12 (we call it damage 13)
- Add the 5% noise when obtaining the SSI data
- Mode Shape Curvature
- Modal Strain energy
- Flexibility matrix

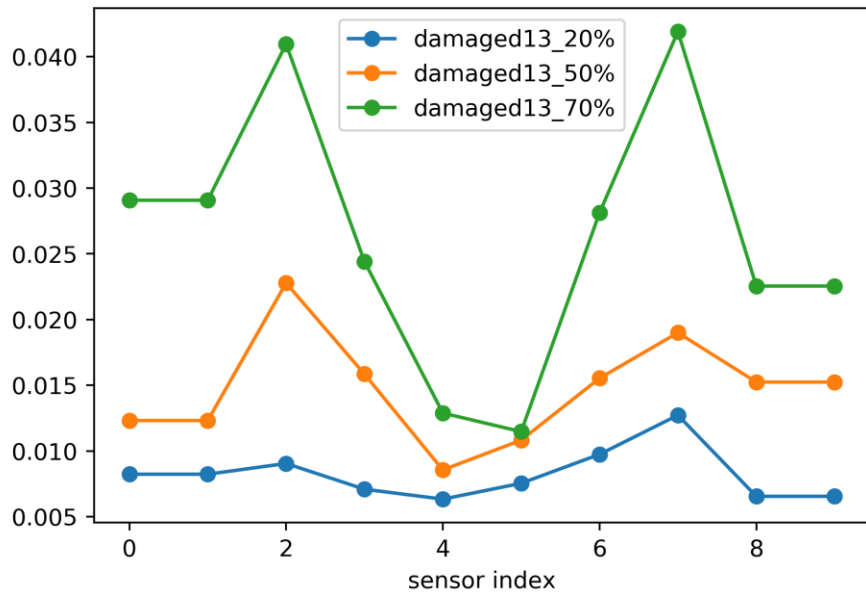
SumofAllOrderabsabsdiff_MSC_SSI2_Uppersensor_y



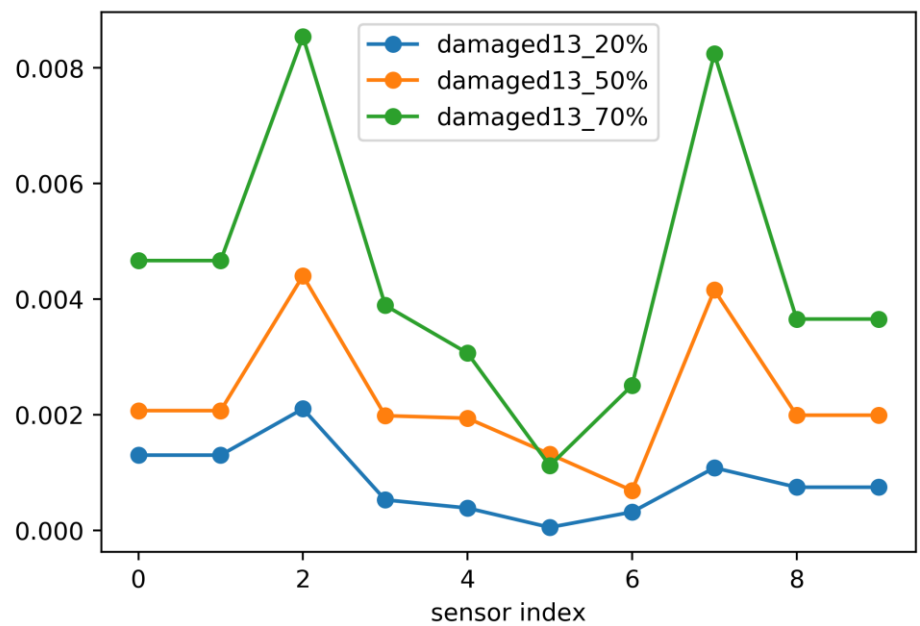
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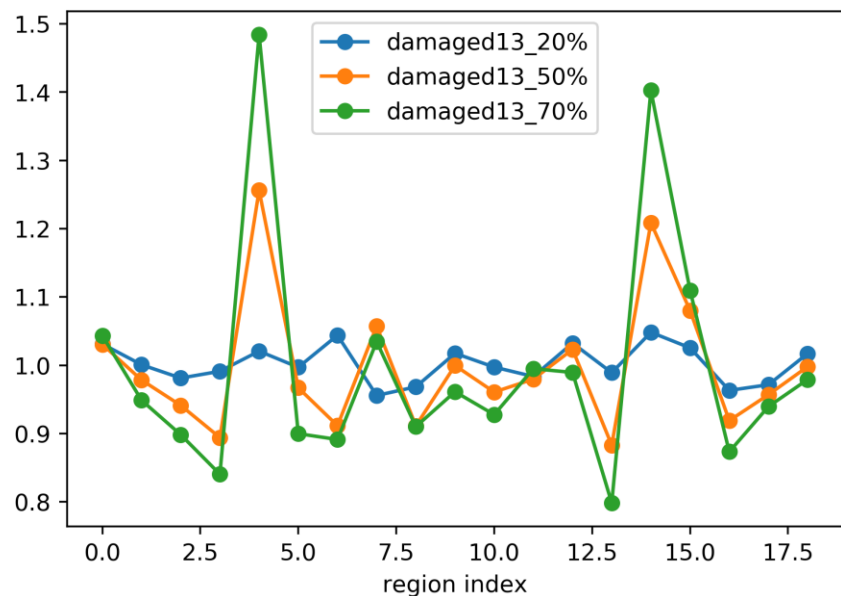
SumofAllOrderabsabsdiff_MSC_SSI2_Uppersensor_y_less10



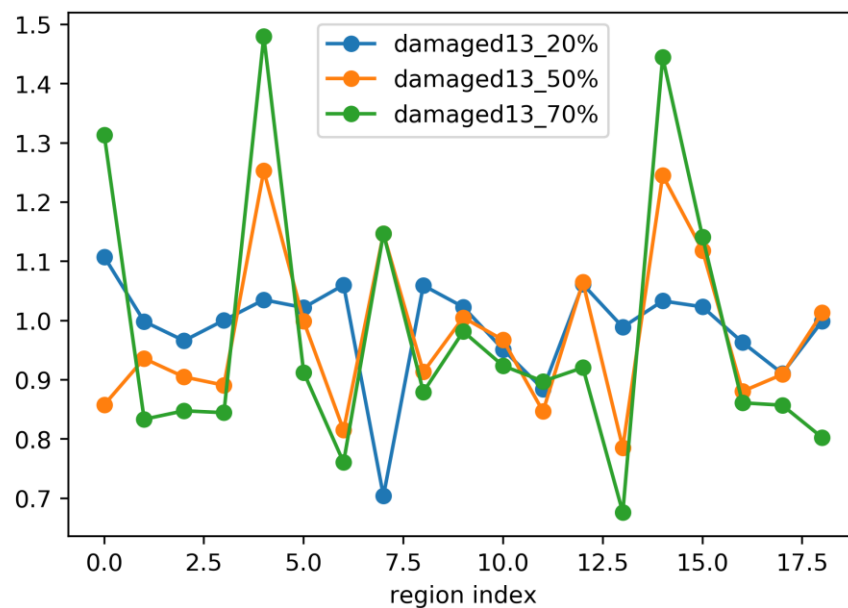
SumofFirstTwoOrderabsabsdiff_MSC_SSI2_Uppersensor_y_less10



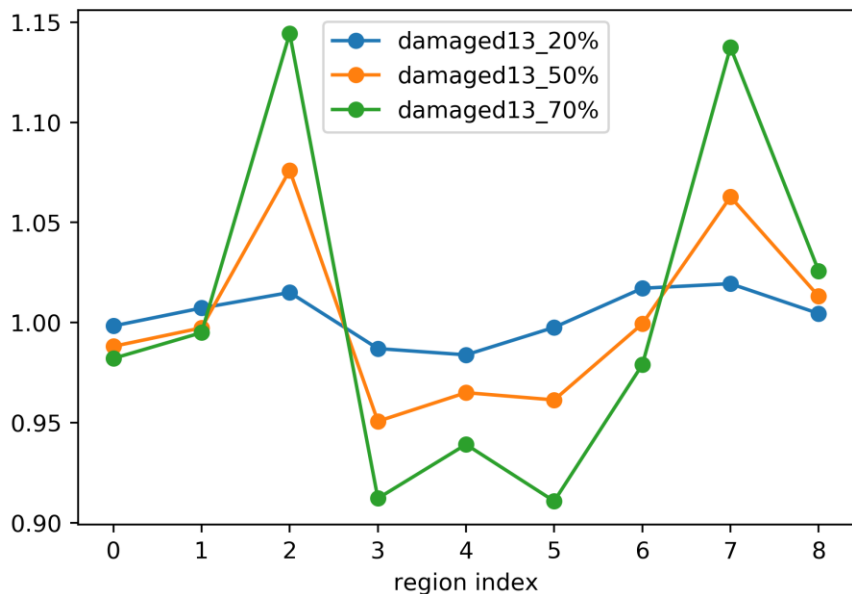
ModalStrainEnergybeta_SSI2_Uppersensor_y



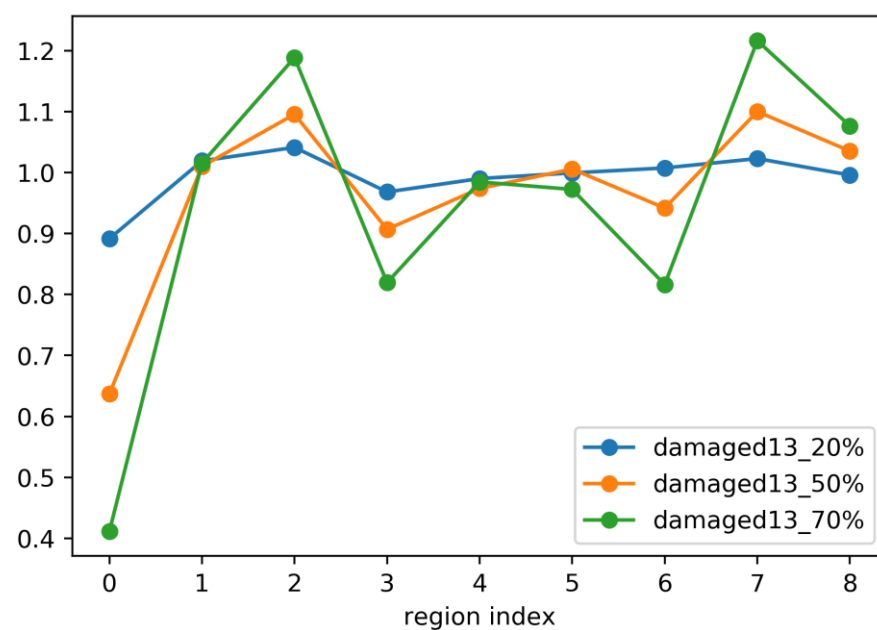
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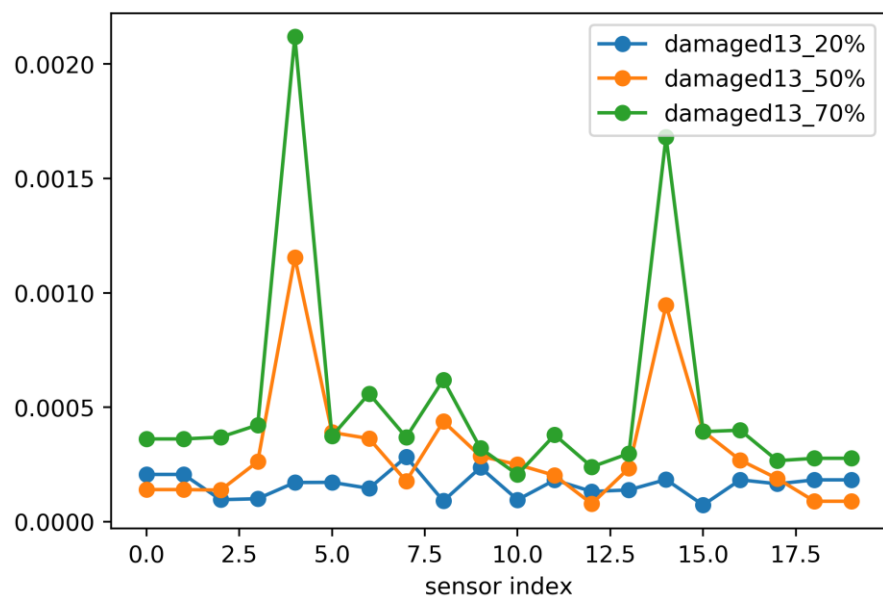
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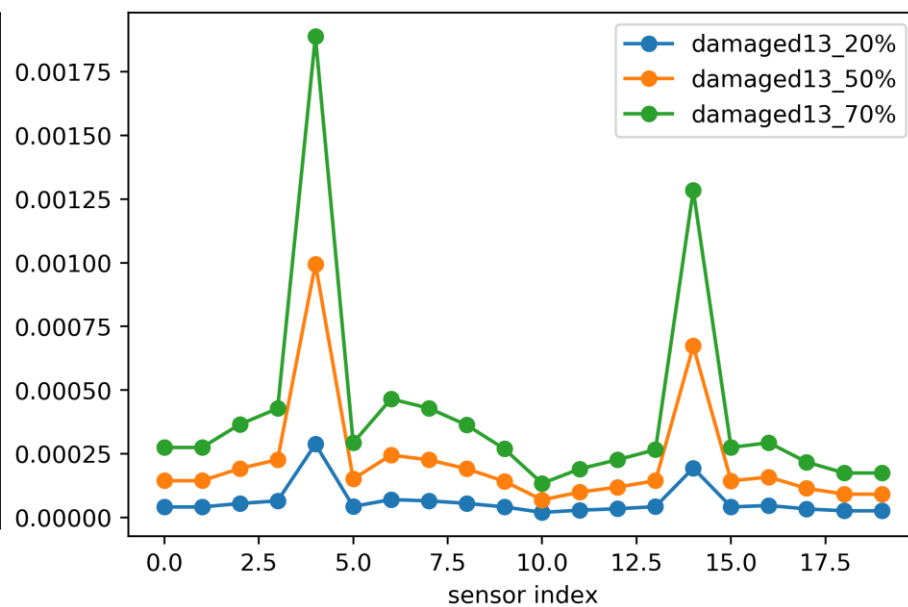
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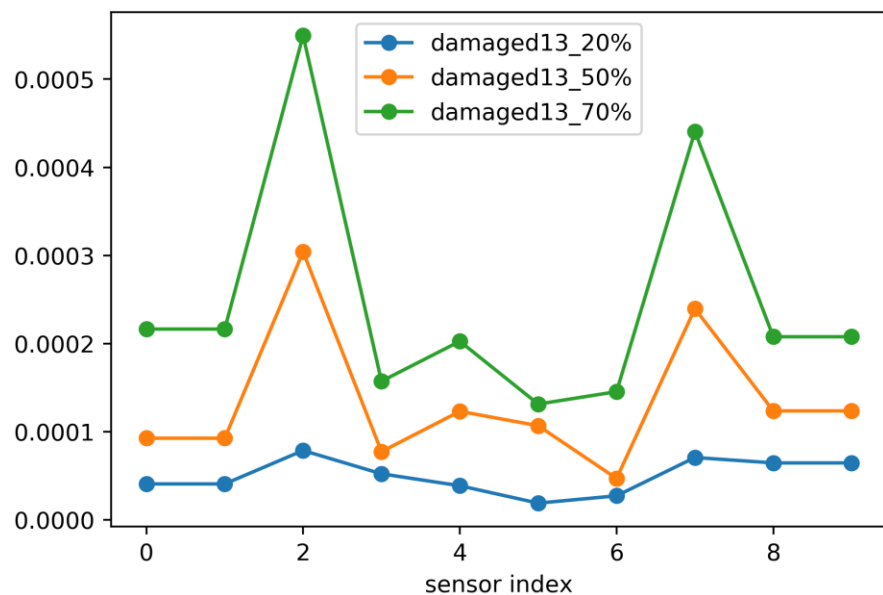
SumofAllOrderabsabsdiffvc_FlexibilityMatrix_SSI2_Uppersensor_y



SumofFirstTwoOrderabsabsdiffvc_FlexibilityMatrix_Modal_Uppersensor_y



SumofAllOrderabsabsdiffvc_FlexibilityMatrix_SSI2_Uppersensor_y_less10



SumofFirstTwoOrderabsabsdiffvc_FlexibilityMatrix_SSI2_Uppersensor_y_less10

